

电感问题知多少，MPS论坛来揭晓

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(特别鸣谢 Sven Spohr)

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1. Introduction

2. Selection of Inductor In DCDC

3. Pain Points of Inductor Using

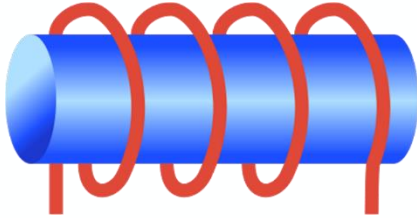
- Saturation Current

- Impact On EMI

4. Conclusions

Introduction - What Is an Inductor?

Wire wounded in coil shape with or without core



What is the main task of the inductor?

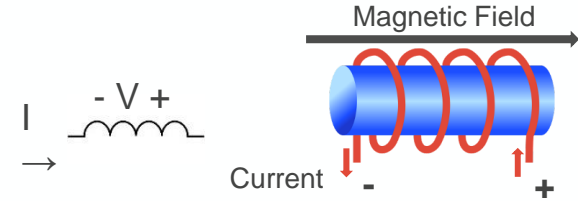
Opposes a change in current

$$V = L \frac{di}{dt}$$

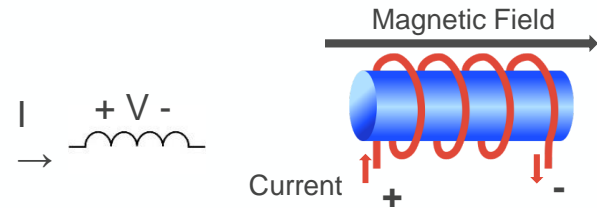
Inductors always have a voltage across them if there is change of current

$$I = \text{constant} \quad \underline{\underline{V = 0}}$$

- It opposes a change in current from a circuit
 - If current is increasing, inductors try to keep them from increasing

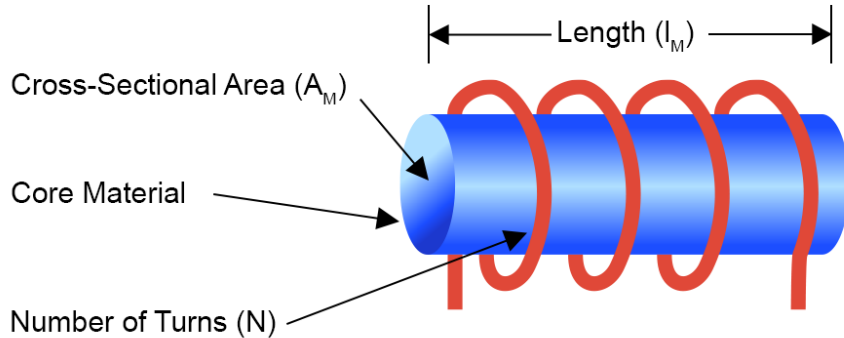


- If current is decreasing, inductors try to keep them from decreasing



Inductance

$$L = \frac{\mu_0 \mu_r A}{l} N^2$$



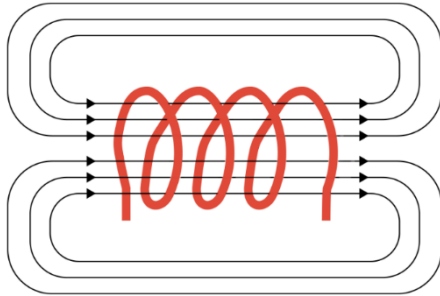
How to Increase Inductance:

- μ ↑ Higher Permeability Core Material
- l ↓ Reduce Effective Length of Core
- A ↑ Bigger Core Cross Sectional Area
- N^2 ↑ Higher Number of Turns

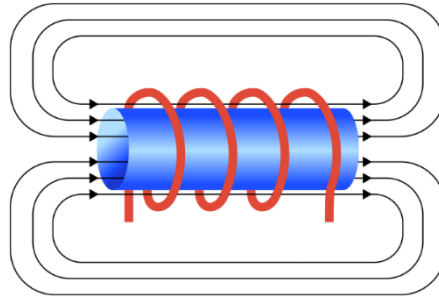
Balance Between Size, Weight, and Performance
Smallest Package Possible to Reduce Weight
Less Turns Possible to Reduce R_{DC}

Permeability

Material	Relative Permeability μ_r
Air	~ 1
Iron (FE-Based)	50 to 150
Nickel-Zinc	40 to 1500
Manganese-Zinc	300 to 20000



$$\vec{B} = \mu_0 \vec{H}$$



$$\vec{B} = \mu_0 \mu_r \vec{H}$$

The magnetic field remains the same

Magnetic flux concentration can intensify by using highly permeable core material

$$L = \frac{\mu_0 \mu_r A}{l} N^2$$

Rated Current

Self-heating of the component caused by the wire's R_{DC} .

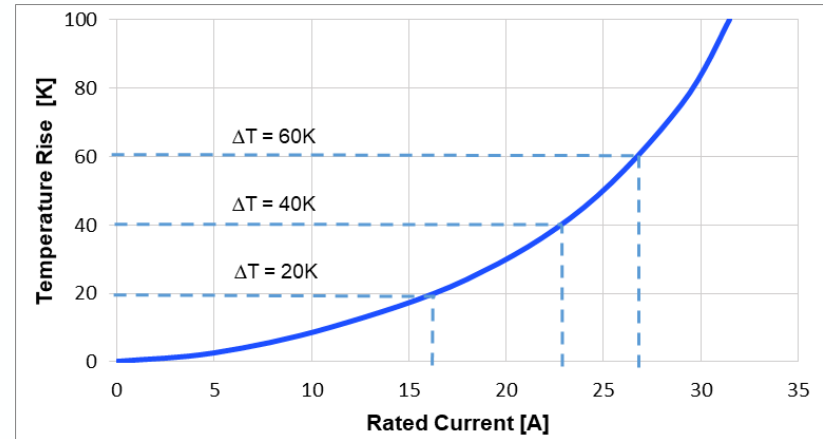
The temperature rise is not standard, and varies from manufacturer to manufacturer.

$$T_{OP} = T_{AMB} + \Delta T$$

T_{AMB}	Ambient Temp	-40 to 85°C / -40 to ?°C
ΔT	Temperature Rise (Self-Heating)	20K / 30K / 40K / ?K
T_{OP}	Operating Temperature	Max. Value Given in Datasheet

Don't exceed the maximum operating temperature T_{OP}

- At higher ambient temperatures, the ΔT (self-heating) should be adjusted
- Larger-sized component

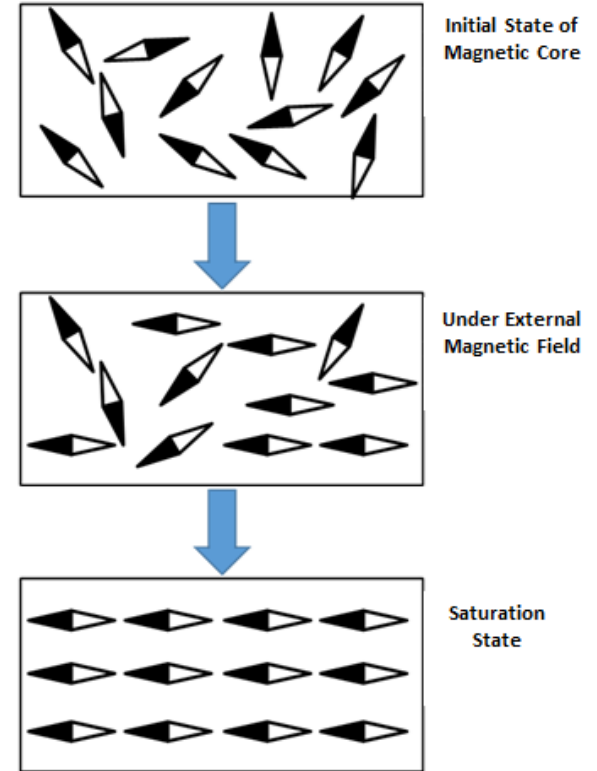
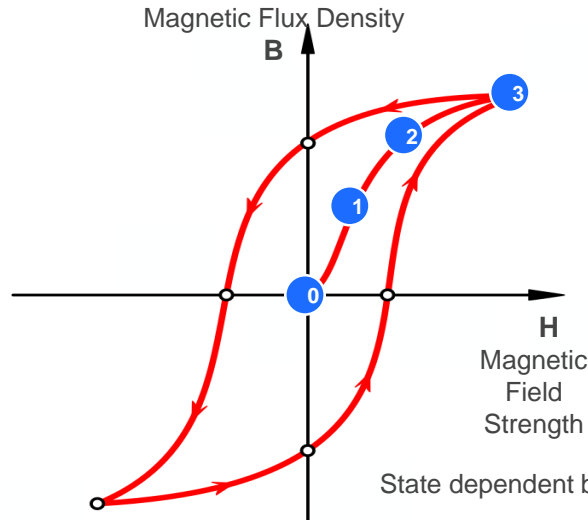


Saturation Current

When the current is passed through the coil, the coil generates a magnetic field.

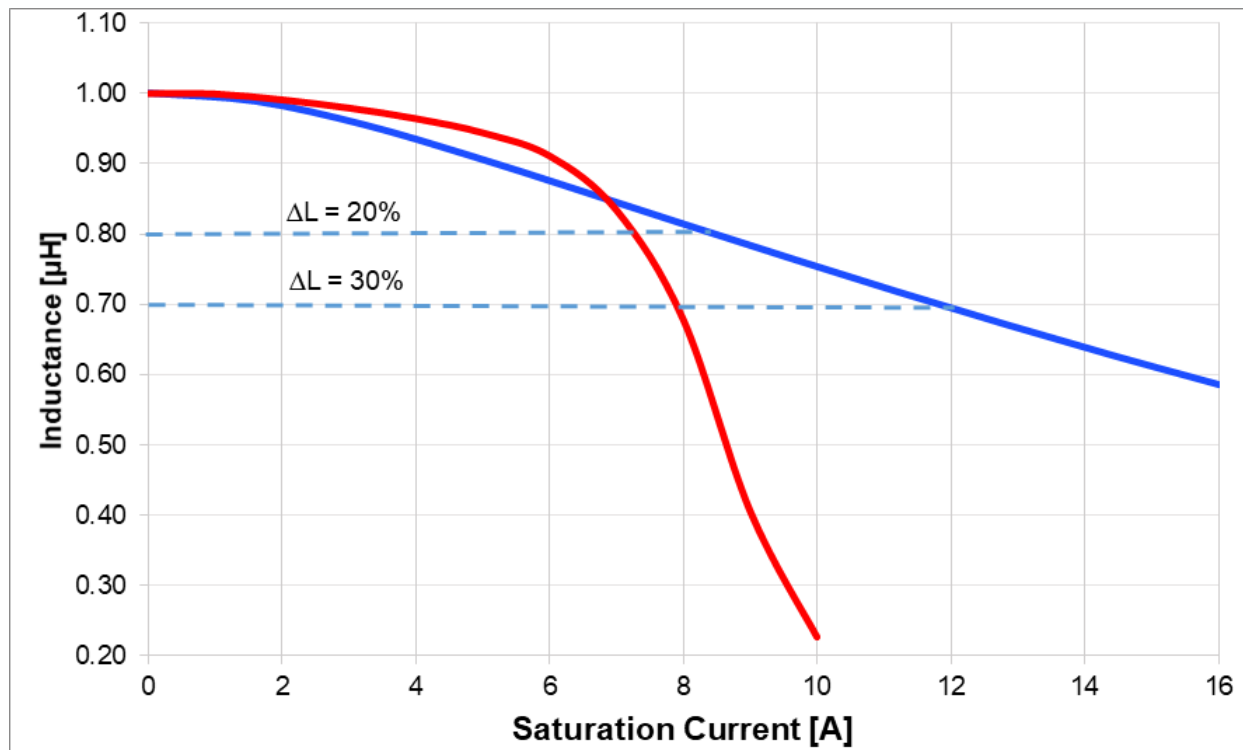
The magnetic core is magnetized by the field, and its internal magnetic domain rotates slowly.

When the magnetic core is completely magnetized, the direction of the magnetic domains becomes consistent with the magnetic field.



Saturation Current

Inductance drops by 30% at the given current

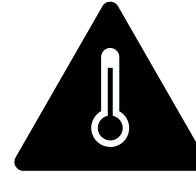


Losses

Copper Losses

DC loss

Heat dissipation of the inductor winding's R_{DC}



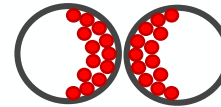
AC loss

Winding structure loss driven by the frequency

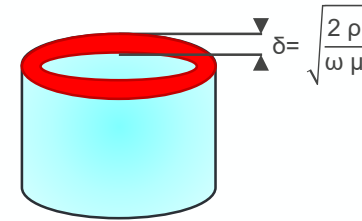
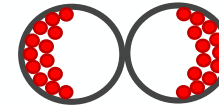
Proximity Effect

Skin Effect

Current in Opposite Direction



Current in Same Direction

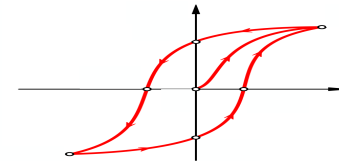
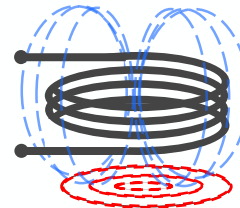


Core Losses

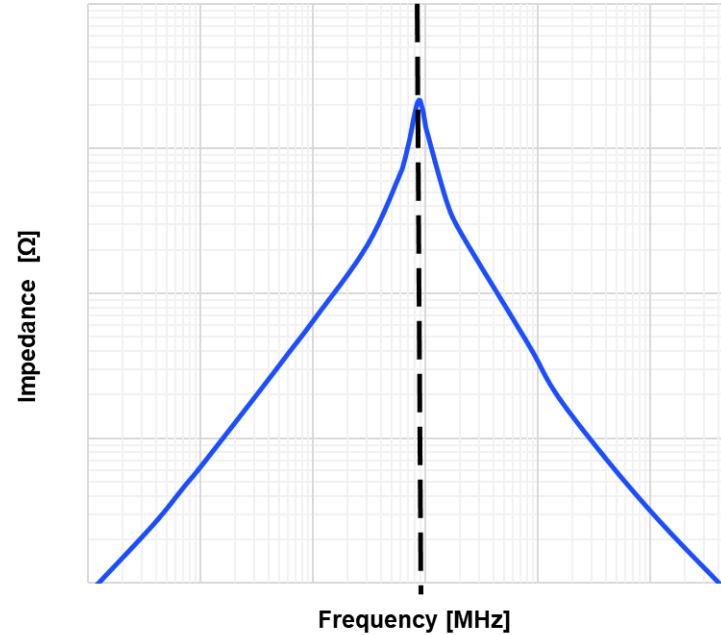
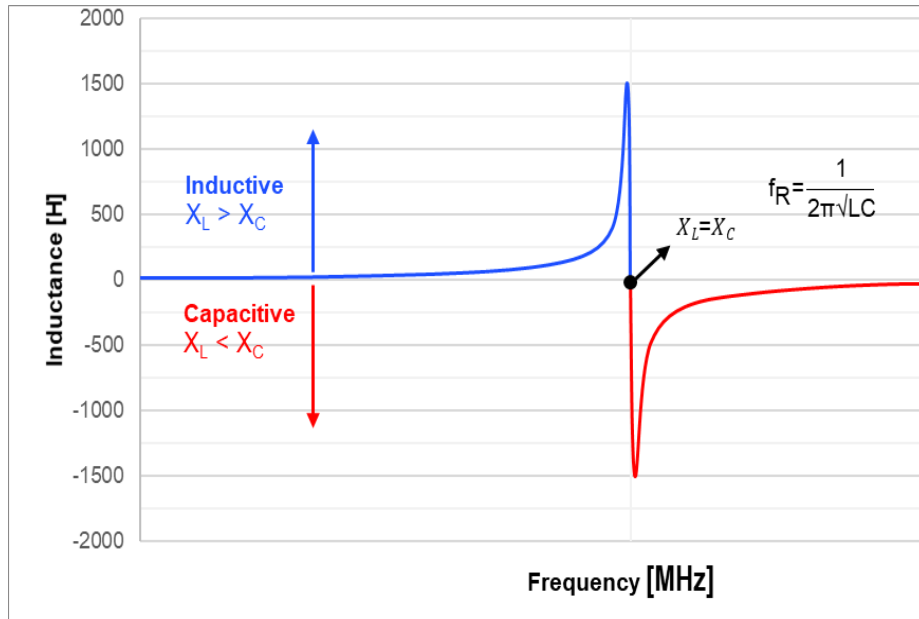
Magnetic material loss

Eddy Currents

Hysteresis Loss



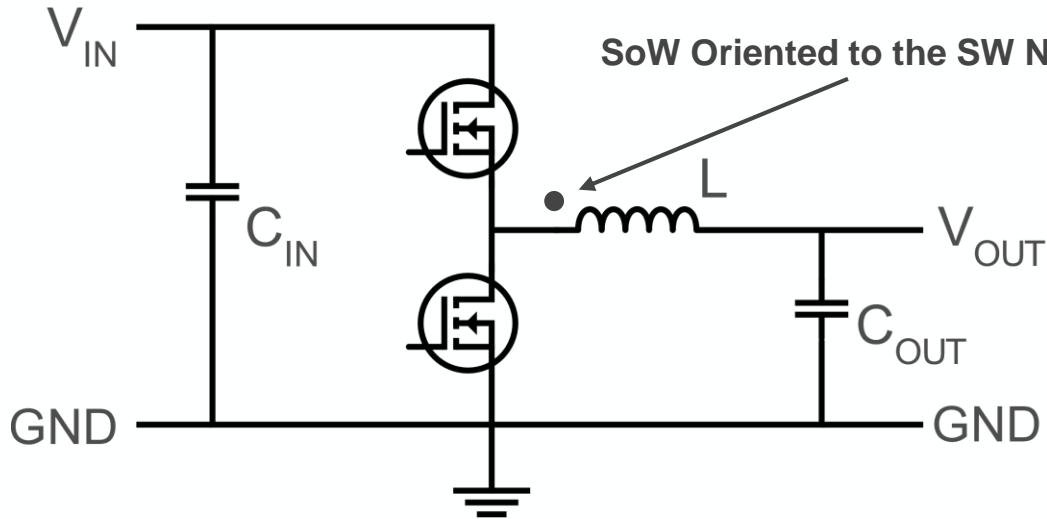
Resonant Frequency



Self-resonant frequency needs to be much higher than the switching frequency

Start of Winding

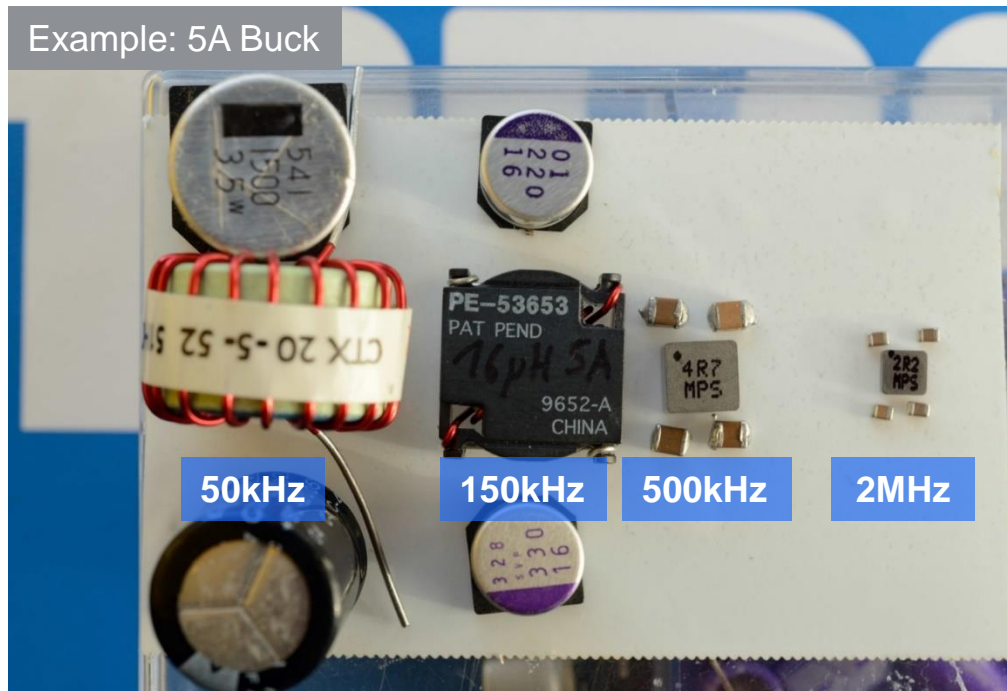
The converter switch node is close to the start of winding side



Selection of Inductor In DCDC

Inductor Selection – Different Switching Frequency

Switching frequency is a key factor to determine how much inductance you use.



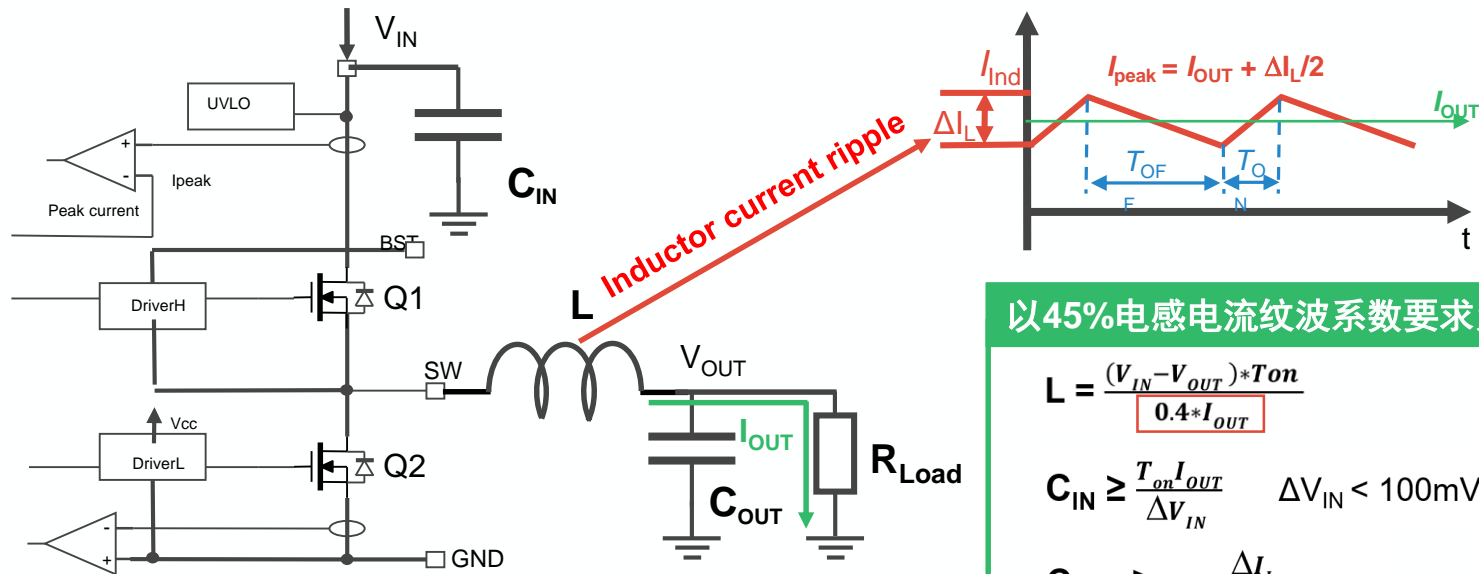
Switching
Frequency



Inductor
Size



Inductor Selection – Current Ripple



以45%电感电流纹波系数要求为例，可得：

$$L = \frac{(V_{IN} - V_{OUT}) * T_{on}}{0.4 * I_{OUT}}$$

$$C_{IN} \geq \frac{T_{on} * I_{OUT}}{\Delta V_{IN}} \quad \Delta V_{IN} < 100\text{mV} \quad \text{ESR} < \frac{\Delta V_{IN}}{I_{peak}}$$

$$C_{OUT} \geq \frac{\Delta I_L}{(8 * F_{SW} * \Delta V_{OUT})}$$

$$\text{ESR} < \frac{\Delta V_{OUT}}{\Delta I_L}$$

V_{OUT} ripple:

$$\Delta V_{OUT} \sim \Delta I_L (\text{ESR} + 1 / (8 * F_{SW} * C_{OUT}))$$

关键设计指标:

- I_{OUT}
- ΔI_L
- ΔV_{IN}
- ΔV_{OUT}

$$\text{Q1 D.C. (Duty Cycle)} = \frac{V_{OUT}}{V_{IN}}$$

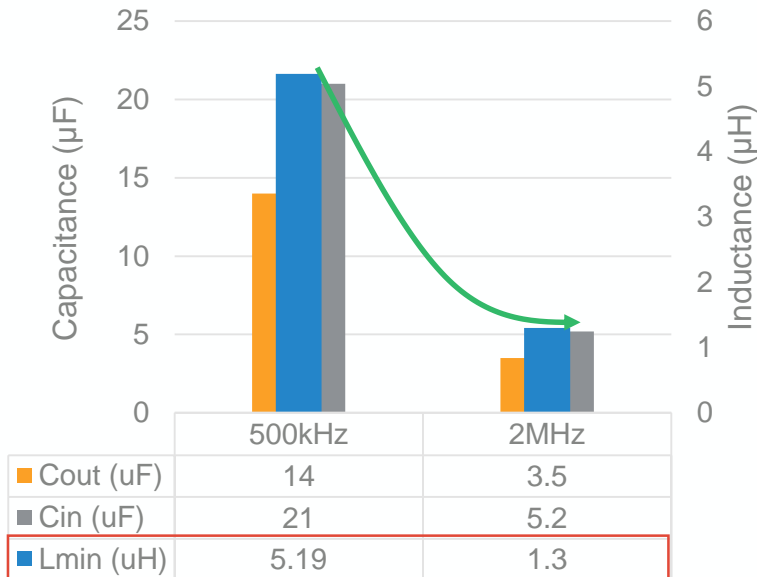
$$T_{ON} = \frac{D.C.}{F_{SW}}$$

Inductor Selection – Working Condition

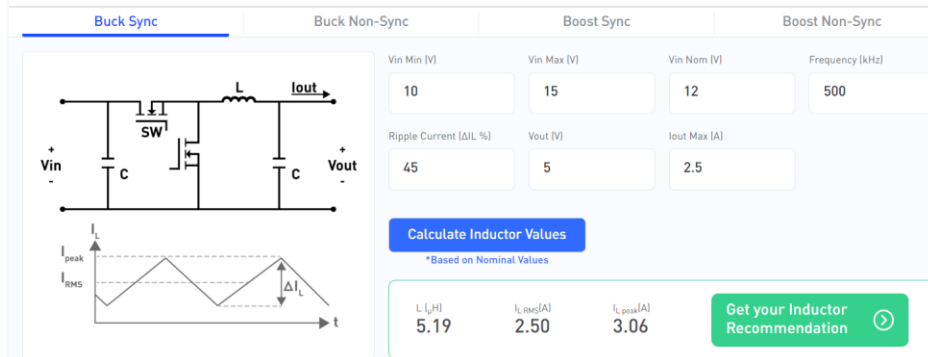
Design Example:

- 45% Inductor Ripple Current
- 20mV Peak-to-Peak Output Ripple
- With $F_s=500\text{kHz} / 2\text{MHz}$
- $V_{in}=12\text{V}$; $V_{out}=5\text{V}$ @ 2.5A

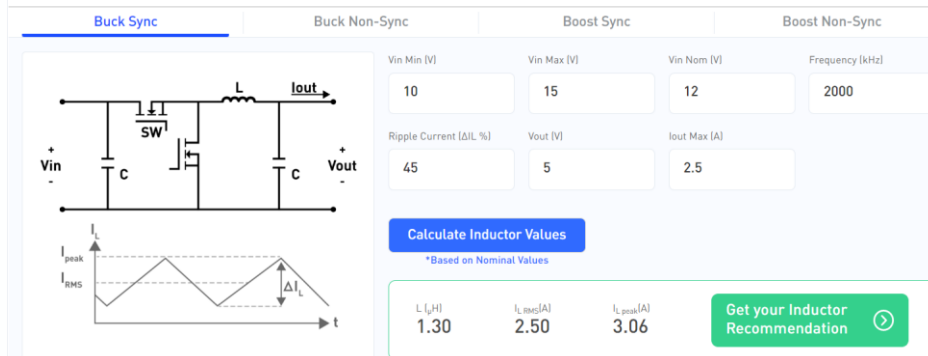
Component Sizing 12V to 5V at 2.5A



Inductor Selector Tool ^



Inductor Selector Tool ^

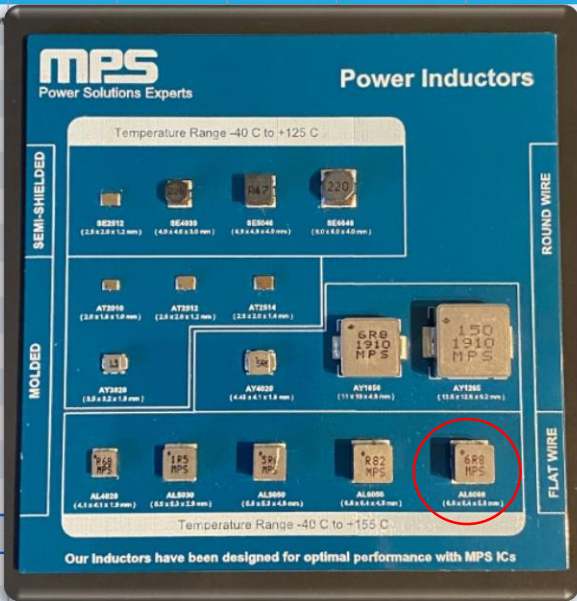


Inductor Selection – MPS Inductor Flyer

MPL Molded Power Inductors

Example
6.8μH / 8.5A

	MPL-AT2010	MPL-AT2512	MPL-AT2514	MPL-AL4020	MPL-AL5030	MPL-AL5050	MPL-AL6050	MPL-AL6060	MPL-AY3020	MPL-AY4020	MPL-AY1050	MPL-AY1265				
Base (mm)	2x1.6	2.5x2	2.5x2	4.1x4.1	5.5x5.3	5.5x5.3	6.6x6.4	6.6x6.4	3.5x3.2	4.45x4.1	11x10	13.5x12.6	Base (mm)			
Height (mm)	1	1.2	1.4	1.9	2.9	4.8	4.8	5.8	1.8	1.8	4.8	6.2	Height (mm)			
	R_{DC} (mΩ)	I_{RMS} (A)	I_{SAT} (A)	R_{DC} (mΩ)	I_{RMS} (A)	I_{SAT} (A)	R_{DC} (mΩ)	I_{RMS} (A)	I_{SAT} (A)	R_{DC} (mΩ)	I_{RMS} (A)	I_{SAT} (A)	R_{DC} (mΩ)	I_{RMS} (A)	I_{SAT} (A)	
0.33μH				13.5	6.4	8.5										0.33μH
0.47μH	27	4.4	5.7	19	5.5	6.4			19.5	6.3	9		1.25	25	41	0.47μH
0.56μH																0.56μH
0.68μH	41	3.5	4.9	26	4.7	6			26	5.15	8.6		1.75	23	36	0.68μH
0.82μH									28	4.7	8		1.3	27	46	0.82μH
1.0μH	50	3.2	4.2	35	4	5.2			30	4.3	6.2		2.6	19	33	1.0μH
1.2μH																1.2μH
1.5μH	97	2.4	3.2	56	3.2	4.2			35	3.4	5.9		3.4	17	26.5	1.5μH
1.8μH																1.8μH
2.2μH	137	2.2	2.7						64	3	5.3		4.9	15	19.5	2.2μH
3.3μH				121	2	2.7			121	2.3	3.7		8	12.5	17	3.3μH
4.7μH	215	1.5	1.9						12	10	9		9.5	11.5	15	4.7μH
5.6μH									13	9	8.6		209	1.8	2.8	5.6μH
6.8μH									16	8.5	8		129	2.2	2.4	6.8μH
8.2μH				280	1.4	2.2			19	8	7		136	2.1	2.1	8.2μH
10μH				355	1.2	1.7			24	6.9	6.6		163	1.9	2	10μH
15μH							37	4.8	35	5.8	5.5					15μH
22μH																22μH

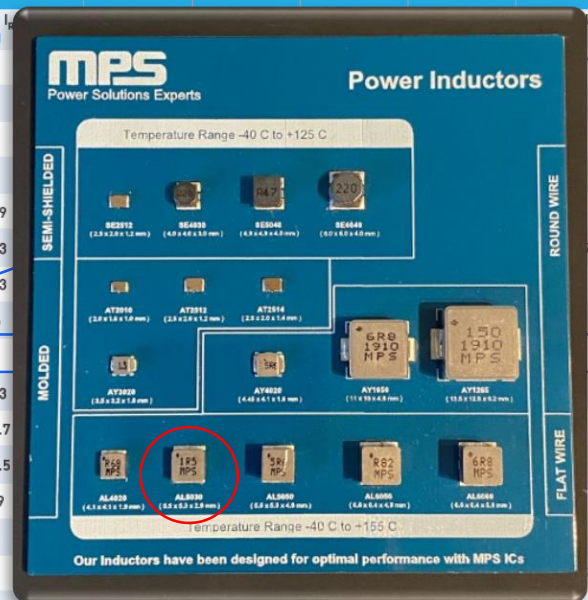


Inductor Selection – MPS Inductor Flyer

MPL Molded Power Inductors

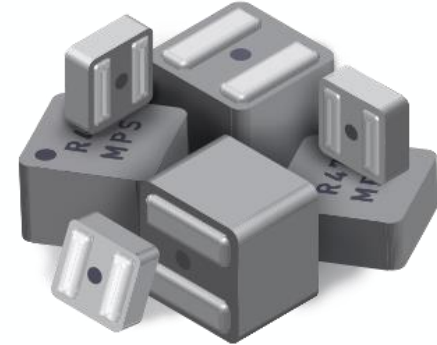
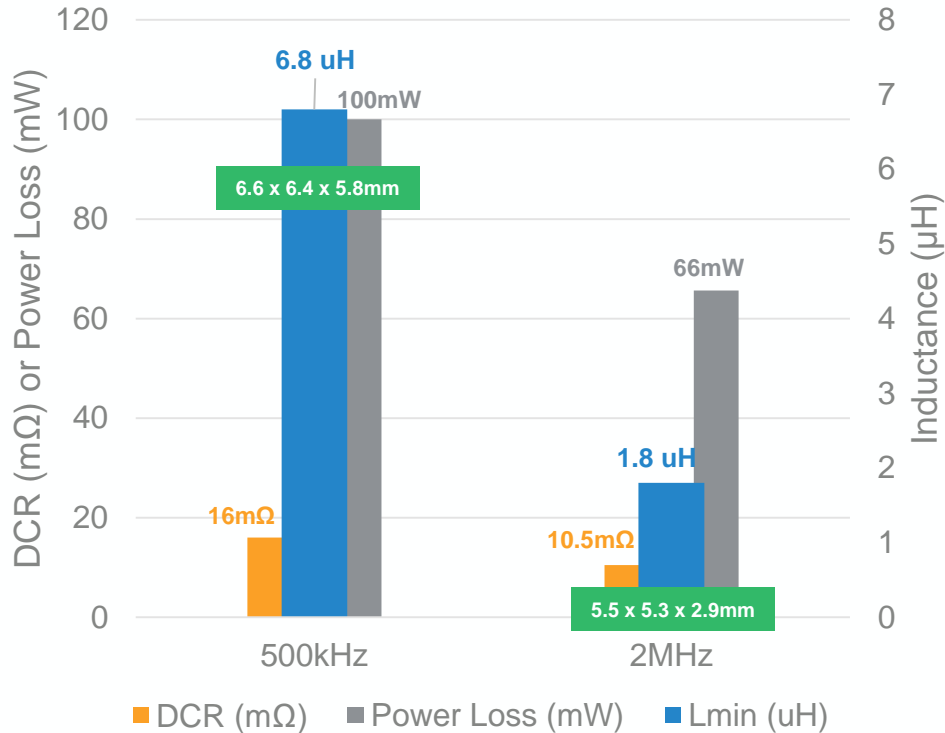
Example
1.8μH / 8.8A

	MPL-AT2010	MPL-AT2512	MPL-AT2514	MPL-AL4020	MPL-AL5030	MPL-AL5050	MPL-AL6050	MPL-AL6060	MPL-AY3020	MPL-AY4020	MPL-AY1050	MPL-AY1265
Base (mm)	2x1.6	2.5x2	2.5x2	4.1x4.1	5.5x5.3	5.5x5.3	6.6x6.4	6.6x6.4	3.5x3.2	4.45x4.1	11x10	13.5x12.6
Height (mm)	1	1.2	1.4	1.9	2.9	4.8	4.8	5.8	1.8	1.8	4.8	6.2
	R _{DC} (mΩ)	I _{RMS} (A)	I _{SAT} (A)	R _{DC} (mΩ)	I _{RMS} (A)	I _{SAT} (A)	R _{DC} (mΩ)	I _{RMS} (A)	I _{SAT} (A)	R _{DC} (mΩ)	I _{RMS} (A)	I _{SAT} (A)
0.33μH												
0.47μH	27	4.4	5.7									
0.56μH												
0.68μH	41	3.5	4.9									
0.82μH												
1.0μH	50	3.2	4.2									
1.2μH												
1.5μH	97	2.4	3.2									
1.8μH					10.5	8.8	12					
2.2μH	137	2.2	2.7									
3.3μH												
4.7μH	215	1.5	1.9									
5.6μH												
6.8μH												
8.2μH												
10μH												
15μH												
22μH												



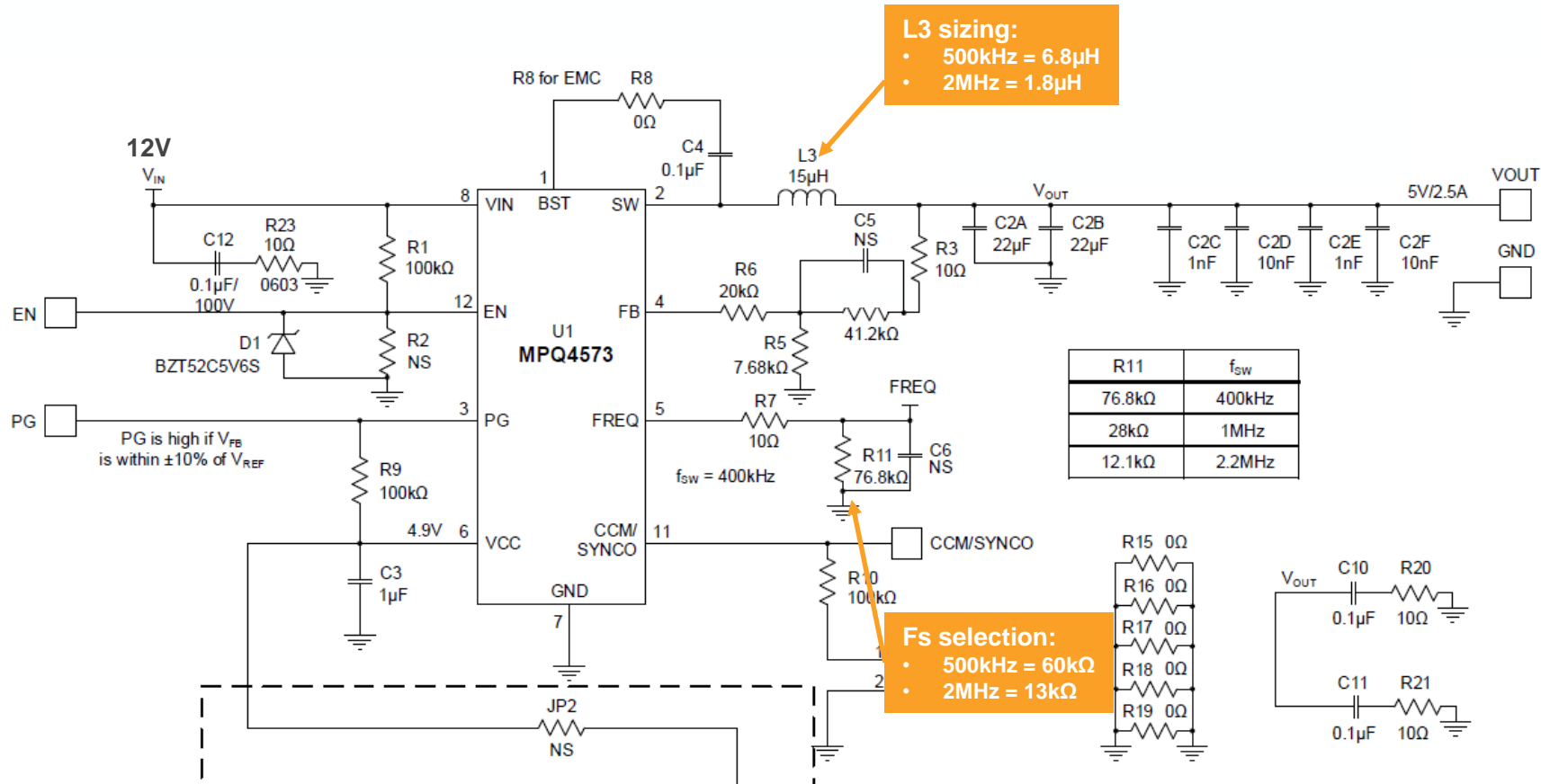
Inductor Selection – MPL-AL Series

Inductor DCR and Power Loss 12V to 5V at 2.5A



- **MPL-AL (Low-Resistance Molded Inductors)**
 - Start of Winding Indication
 - Flat Wire Construction
 - Lowest DCR
 - High Performance
 - High Saturation Current
 - Soft Saturation
 - Stable over Temperature
 - Max Operating Temperature: 155°C
 - Sizes: 4020 / 5030 / 5050 / 6050 / 6060

Inductor Selection – Example On MPQ4573 Demo



L3 sizing:

- 500kHz = 6.8 μ H
- 2MHz = 1.8 μ H

R11	f_{sw}
76.8k Ω	400kHz
28k Ω	1MHz
12.1k Ω	2.2MHz

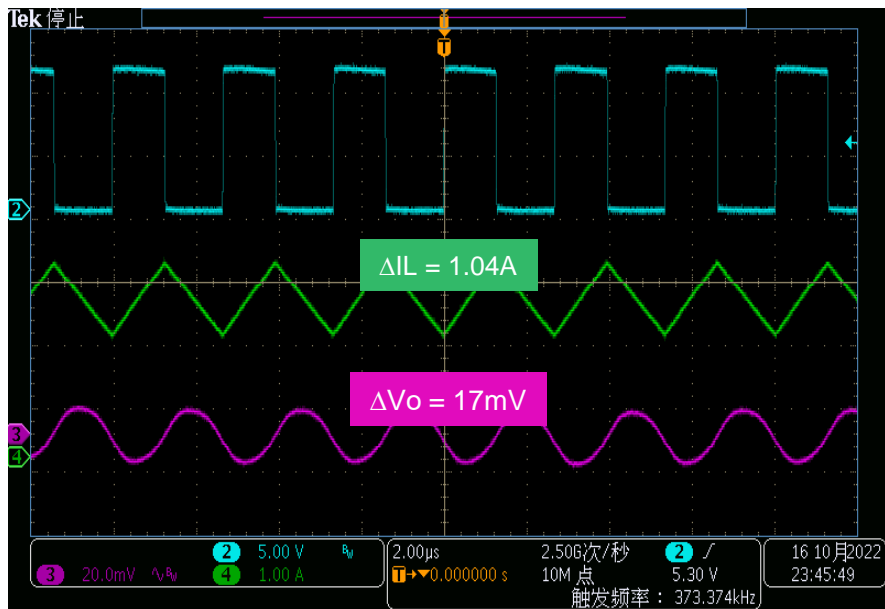
Fs selection:

- 500kHz = 60k Ω
- 2MHz = 13k Ω

Inductor Selection – 500kHz Waveforms

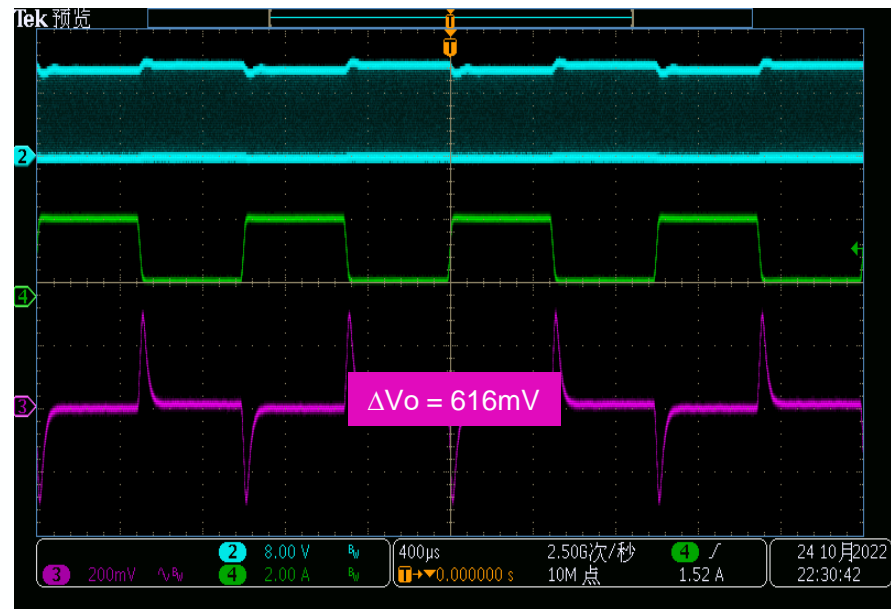
测试条件：12V to 5V @ 2.5A

- $L = 6.8 \mu\text{H}$ (16mOhm)
- 89.74% Efficiency
- $\Delta I_L = 1.04\text{A}$ (42%)



Load=2.5A

Transient can be optimized with more Cout / Compensation.

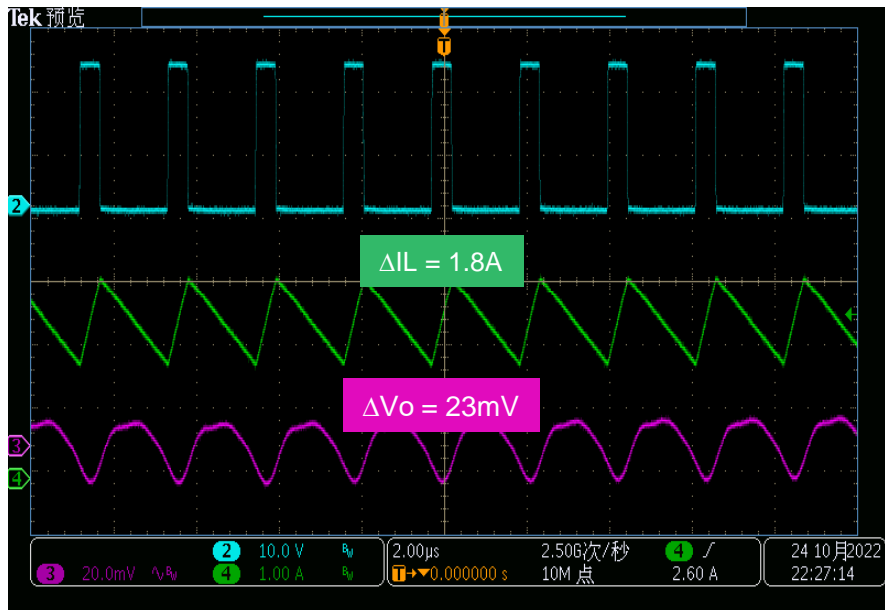


Transient=0.5A to 2.5A

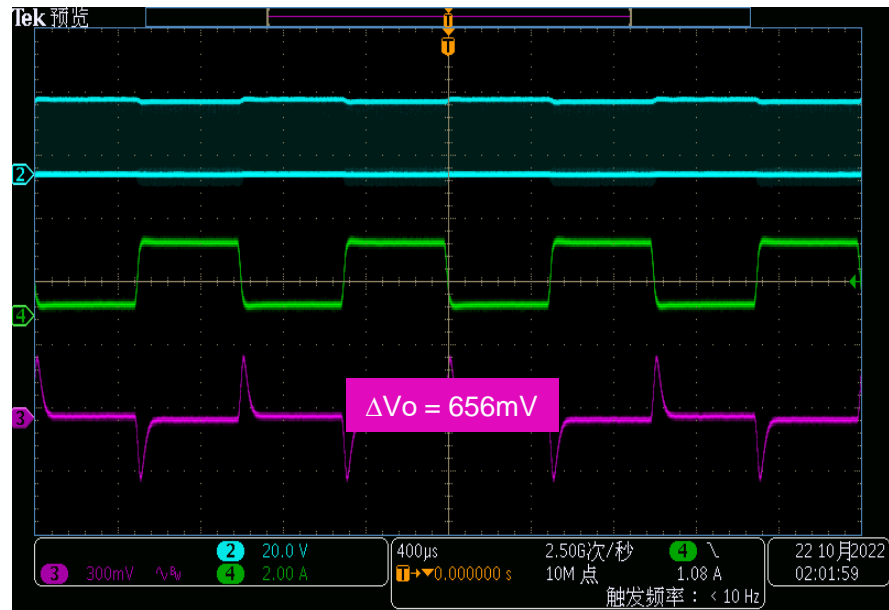
Inductor Selection – 500kHz Waveforms

测试条件：24V to 5V @ 2.5A

- $L = 6.8 \mu\text{H}$ (16mOhm)
- $\Delta I_L = 1.125\text{A}$ (45%)
- Real $\Delta I_L = 1.8\text{A}$ (72%)



Load=2.5A

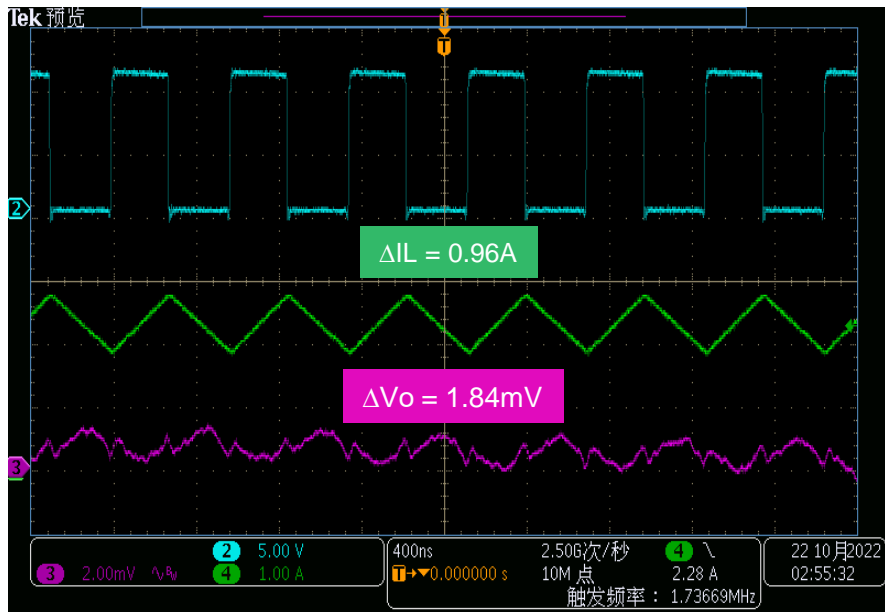


Transient=0.5A to 2.5A

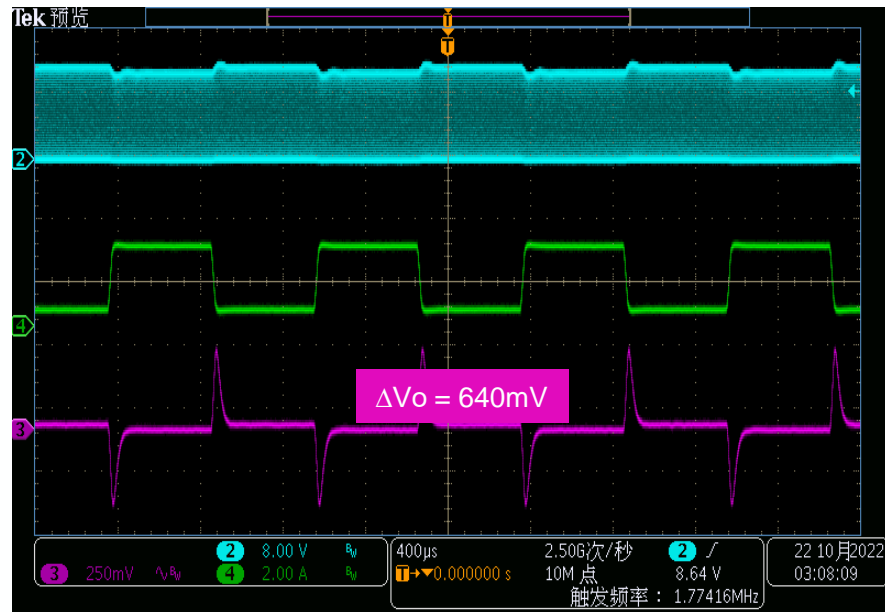
Inductor Selection – 2MHz Waveforms

测试条件：12V to 5V @ 2.5A

- $L = 1.8 \mu\text{H}$ (10.5mOhm)
- 83.82% Efficiency
- $\Delta I_L = 0.96\text{A}$ (38%)



Load=2.5A

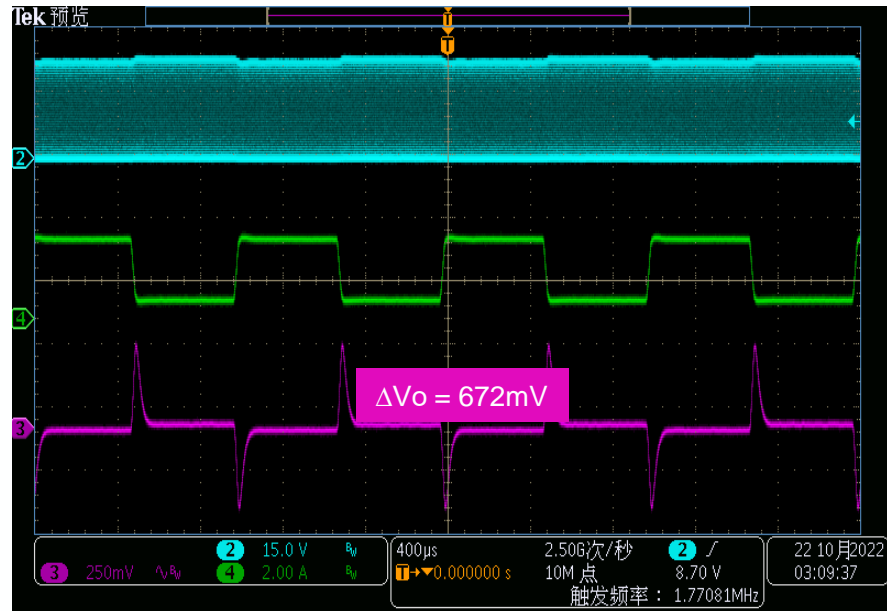
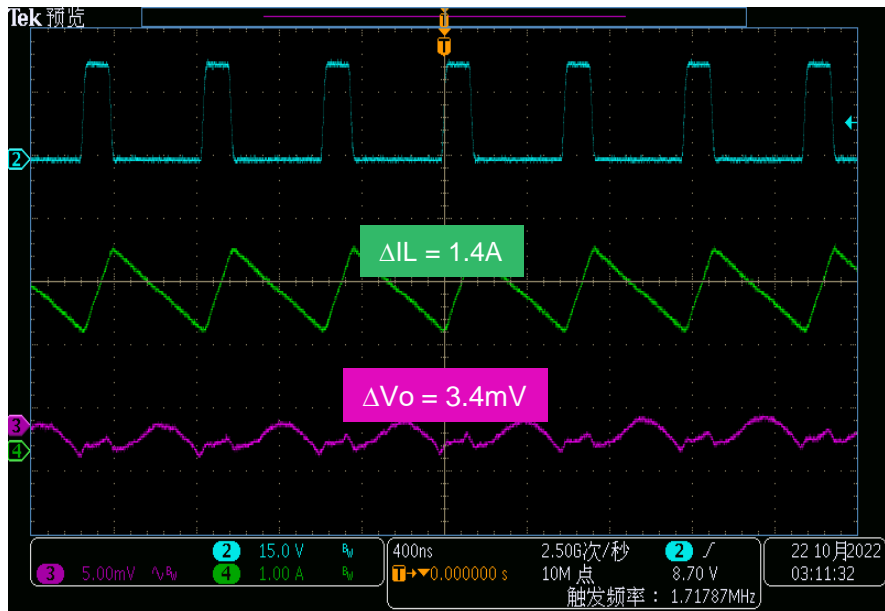


Transient=0.5A to 2.5A

Inductor Selection – 2MHz Waveforms

测试条件：24V to 5V @ 2.5A

- $L = 1.8 \mu\text{H}$ (10.5mOhm)
- $\Delta I_L = 1.125\text{A}$ (45%)
- Real $\Delta I_L = 1.4\text{A}$ (56%)



Inductor Selection – Efficiency Curve

Efficiency Curve of MPQ4573

(60V, 2.5A sync Buck -
250mΩ/45mΩ $R_{DS(ON)}$)

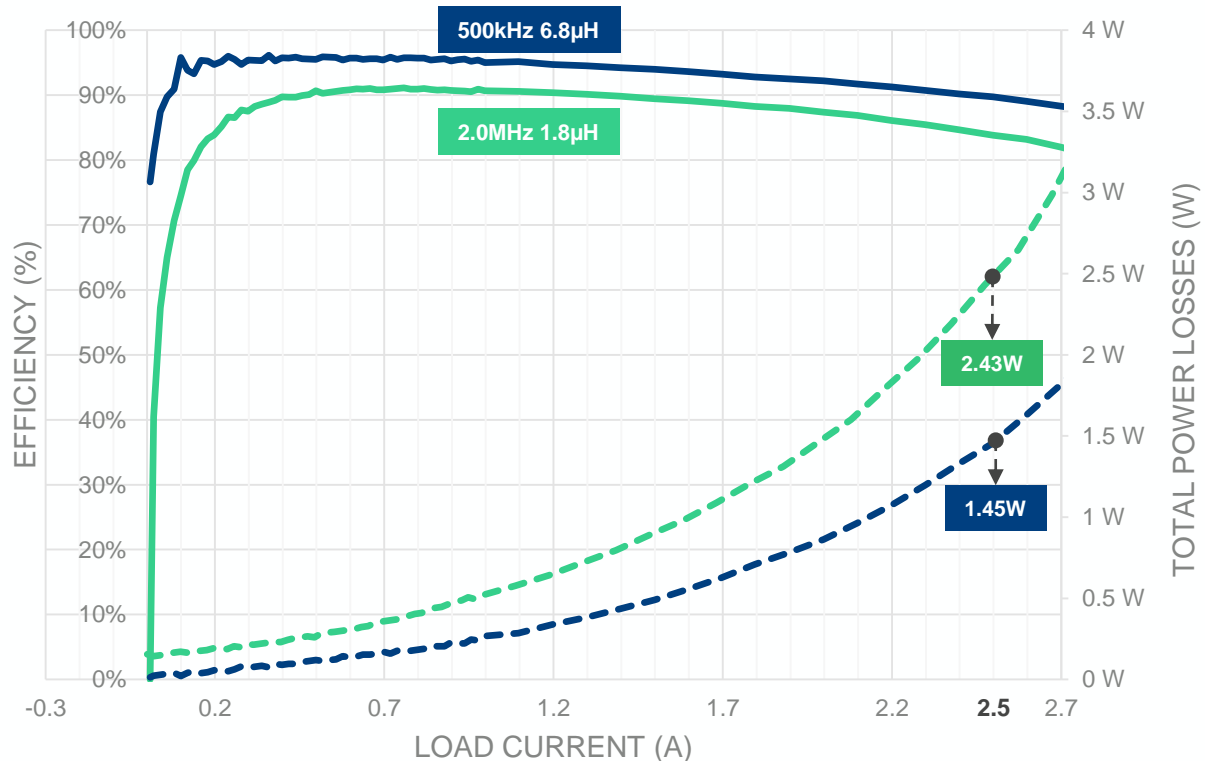
- Calculation shows highest DCR loss in coil for 500kHz setup
- Real world **500kHz efficiency is higher** because of less switch transition losses

Example:

How to losses split up?

1.45W (500kHz@2.5A):

- ✓ IC-FET R_{ON} : 823mW
- ✓ Coil DCR: 100mW
- ✓ Transition losses and IC supply losses: 134mW
- ✓ Others (Core + AC Winding + EMI Filter): 290mW



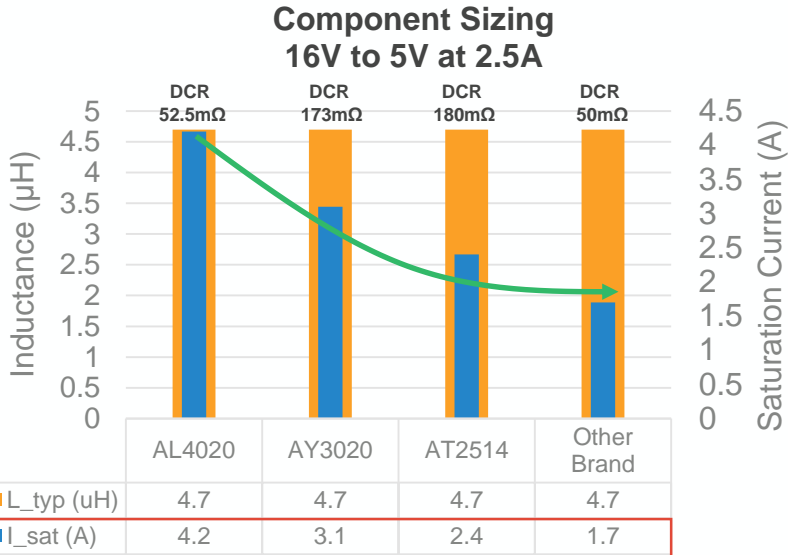
Pain Points of Inductor Using

Saturation Current

Inductor Saturation Current

Design Example (MVQ4573 Demo Board):

- 75% Inductor Ripple Current
- With $F_s=500\text{kHz}$
- $V_{in}=16\text{V}$; $V_{out}=5\text{V}$ @ 2.5A



Inductor Selector Tool ^

Buck Sync

Input	Buck Non-Sync	Boost Sync	Boost Non-Sync
Vin Min [V]	10	18	16
Vin Max [V]			
Vin Nom [V]			
Frequency [kHz]			500
Ripple Current (ΔIL) %	75		
Vout [V]	3.3		
Iout Max [A]		2.5	

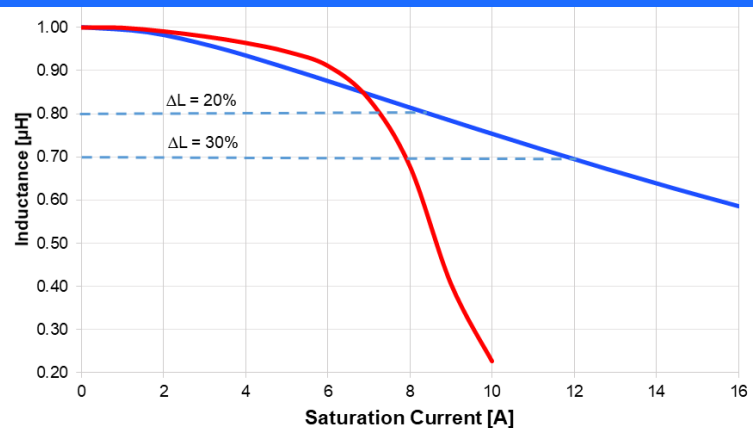
[Calculate Inductor Values](#)

*Based on Nominal Values

$L_{L,HL}$ [uH]	$L_{L,RMS}$ [mH]	$L_{L,peak}$ [mH]
2.79	2.50	3.44

[Get your Inductor Recommendation](#)

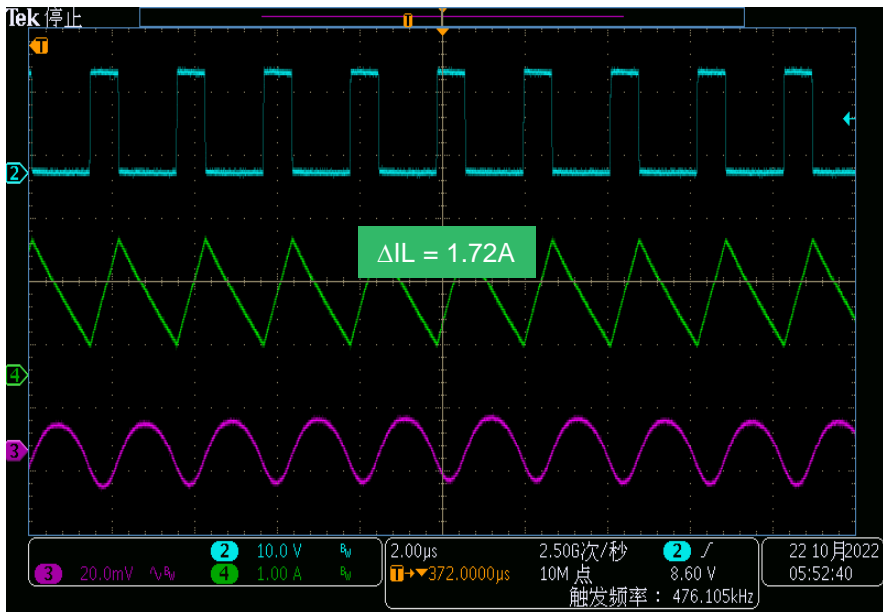
Inductance drops by 30% at the given current



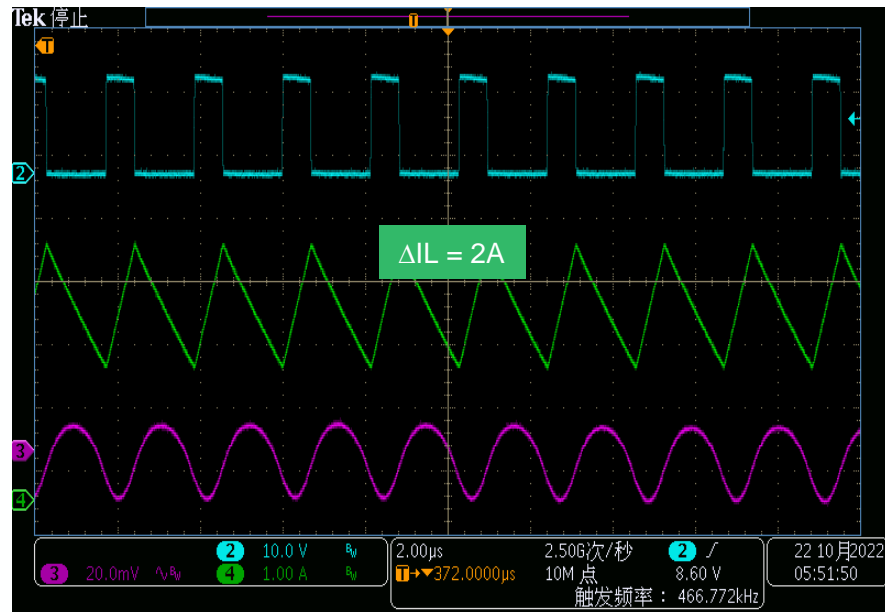
Current Ripple Comparison – AL4020

Test Condition: 16V to 5V

- $L = 4.7 \mu\text{H}$ (52.5mOhm)
- $I_{\text{Sat}}=4.2\text{A}$
- **OCP Threshold: 2.9A (11% ripple change)**



Load=1.25A

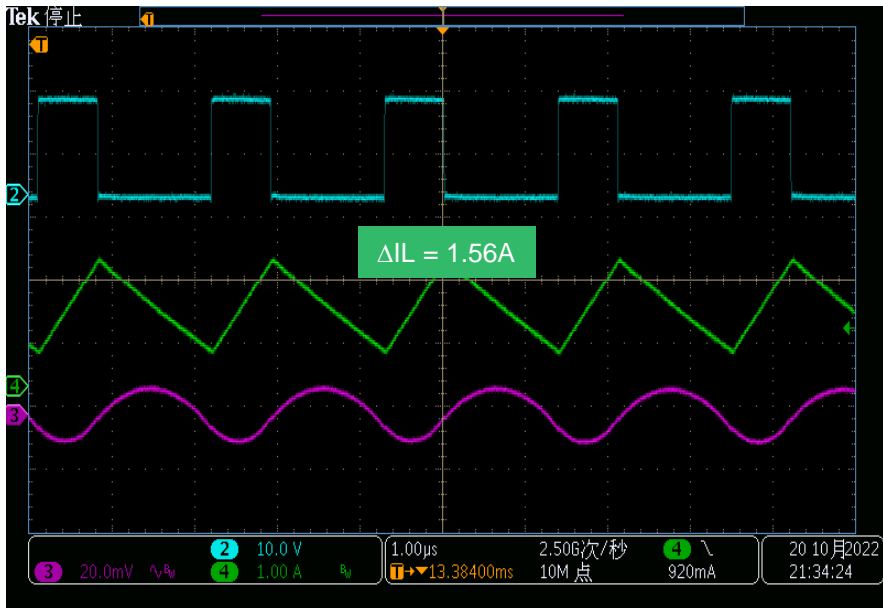


Load=2.9A

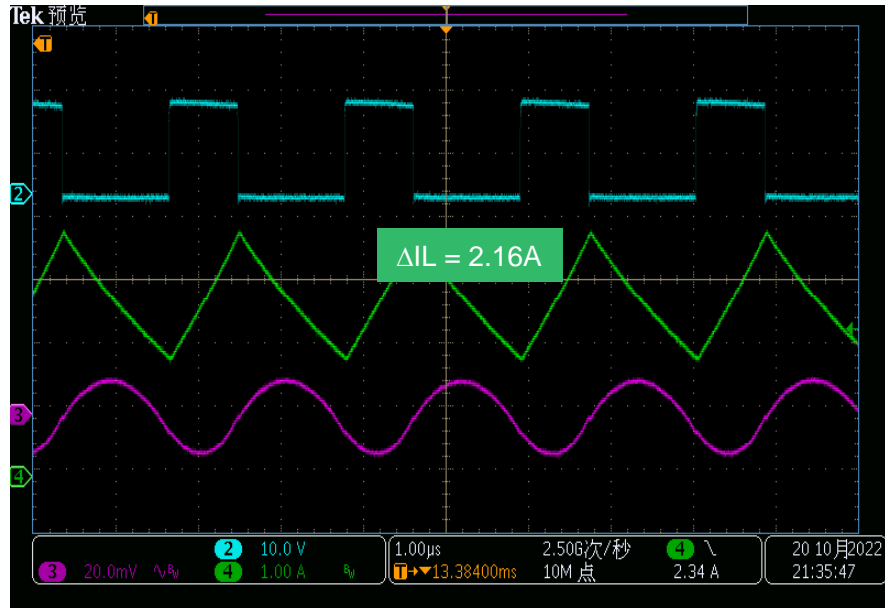
Current Ripple Comparison – AY3020

Test Condition: 16V to 5V

- L = 4.7 μ H (173mOhm)
- I_Sat=3.1A
- **OCP Threshold: 2.8A (24% ripple change)**



Load=1.25A

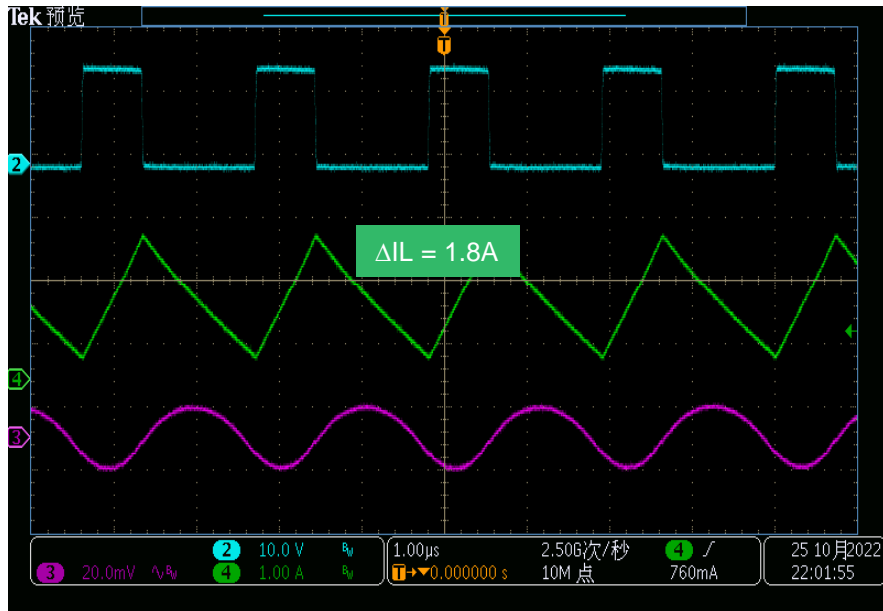
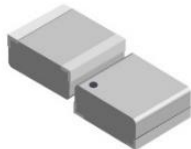


Load=2.8A

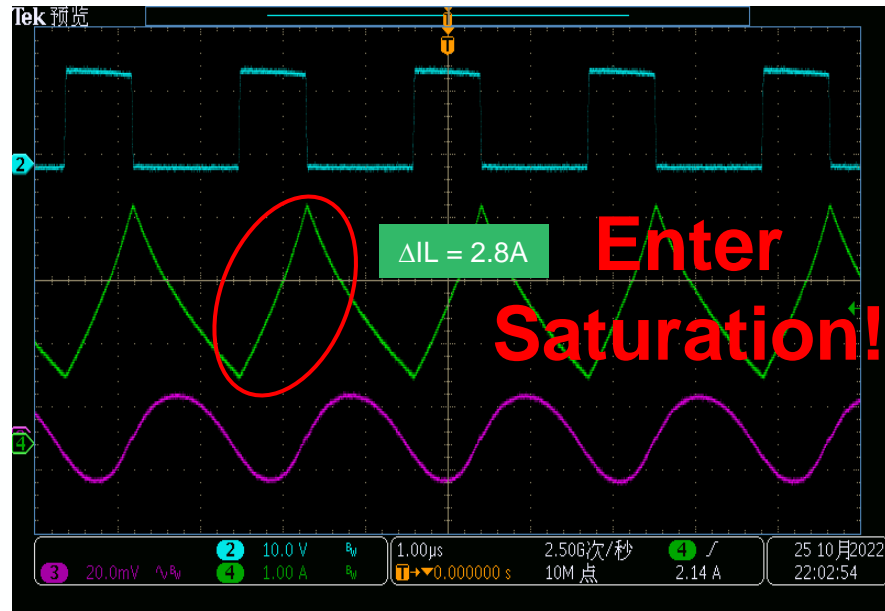
Current Ripple Comparison – AT2514

Test Condition: 16V to 5V

- $L = 4.7 \mu\text{H}$ (180mOhm)
- $I_{\text{Sat}} = 2.4\text{A}$
- **OCP Threshold: 2.8A** (40% ripple change)



Load=1.25A

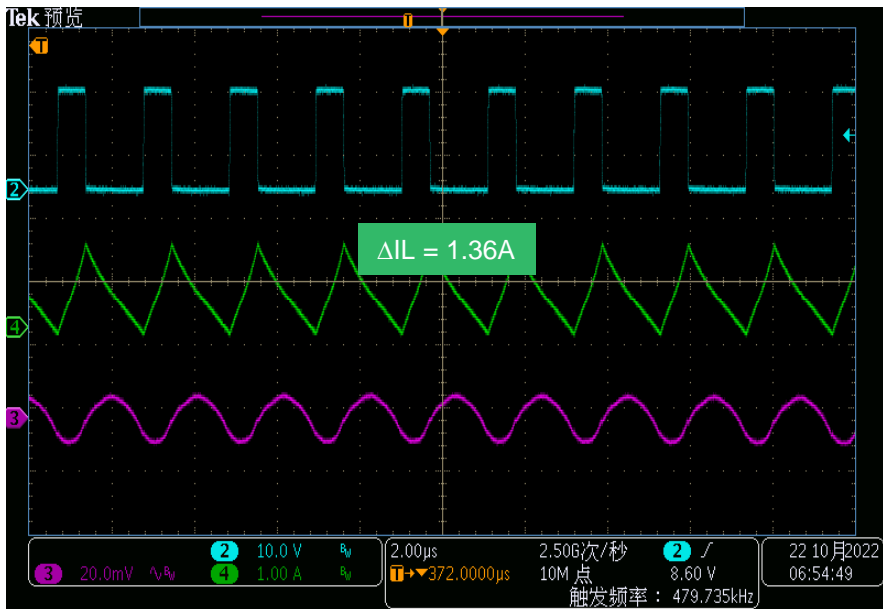


Load=2.2A

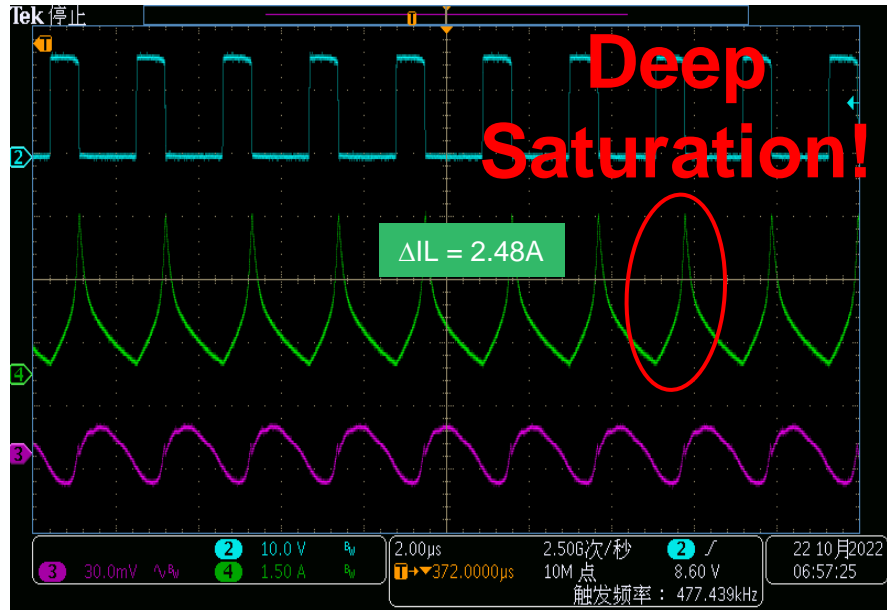
Current Ripple Comparison – Other Brand

Test Condition: 16V to 5V

- L = 4.7 μ H (50mOhm)
- I_Sat=1.7A
- **OCP Threshold: 1.1A**



Load=0.5A

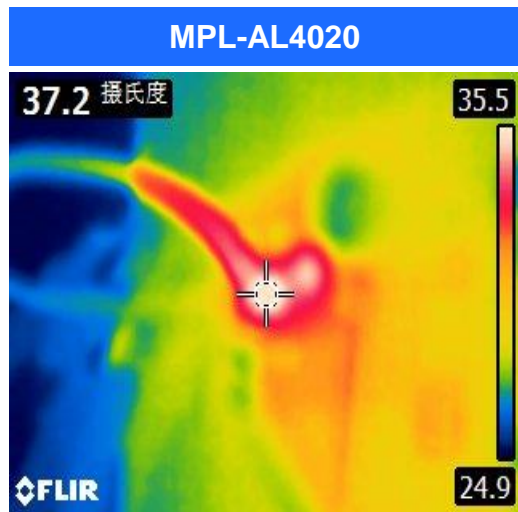


Load=1.1A

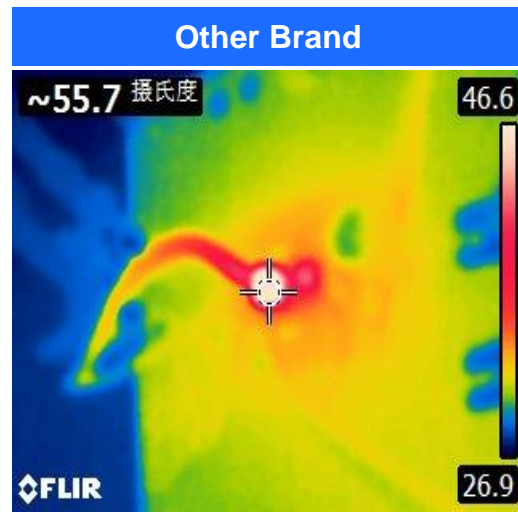
Saturation Condition: Thermal Rising

Test Condition: 16V to 5V

- L = 4.7 μ H (AL4020 & Other Brand)
- Ambient temperature: 26°C



Load=1.1A



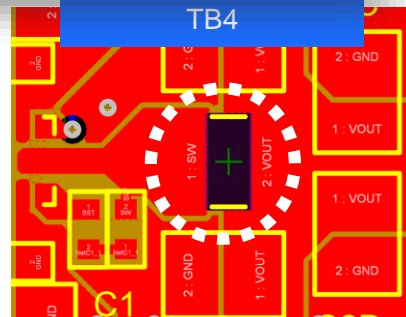
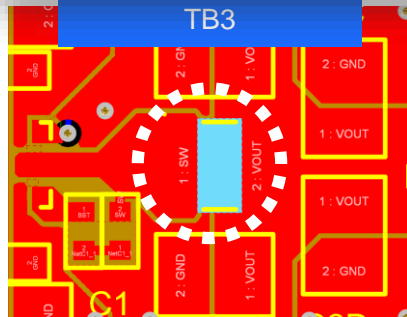
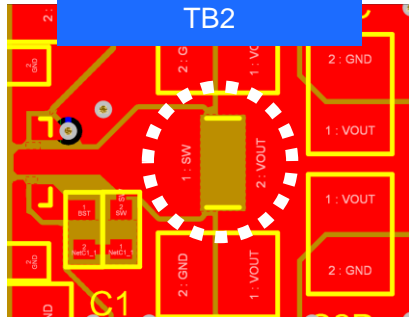
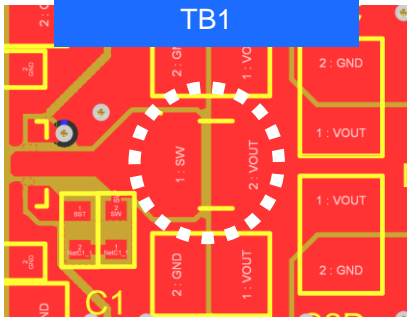
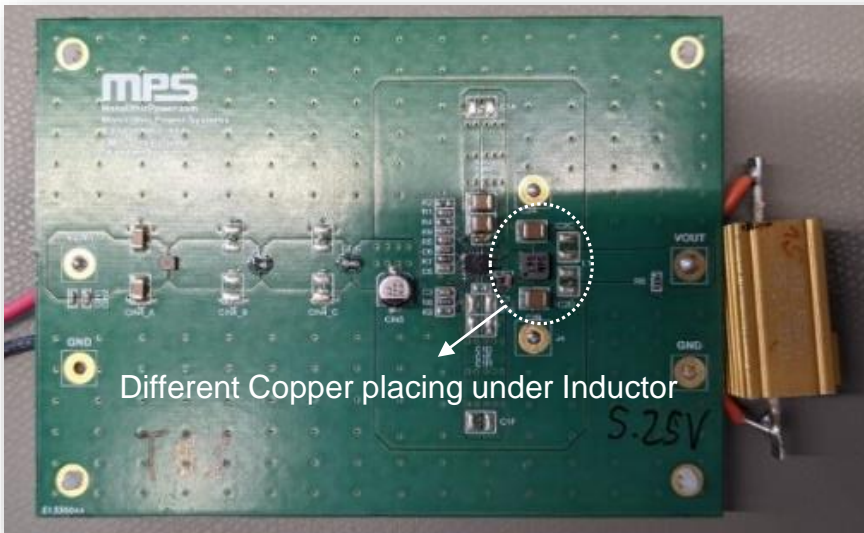
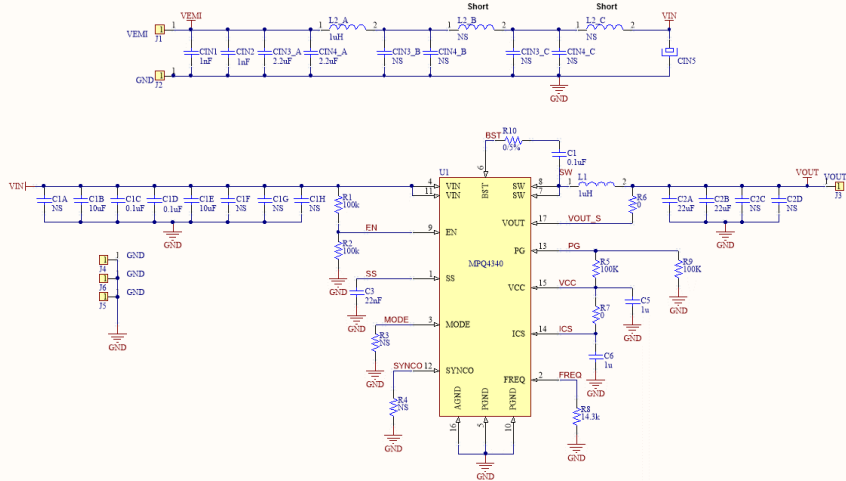
Load=1.1A

Pain Points of Inductor Using

Impact of EMI

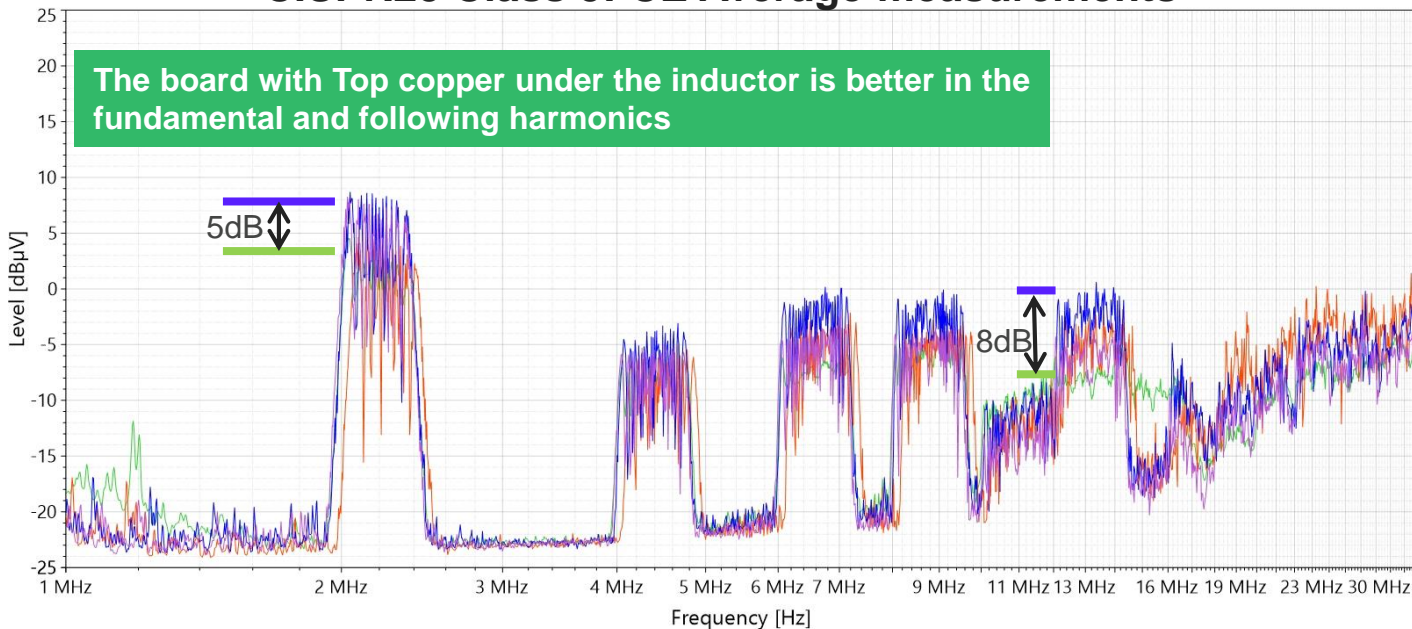
Copper Under The Inductor

Standard Reference Schematics



Copper Under The Inductor: Test results

CISPR25 Class 5: CE Average measurements



TB1: Copper under L

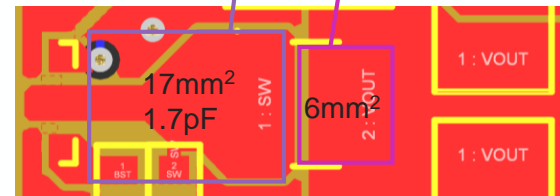
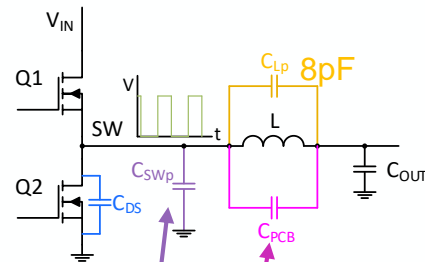
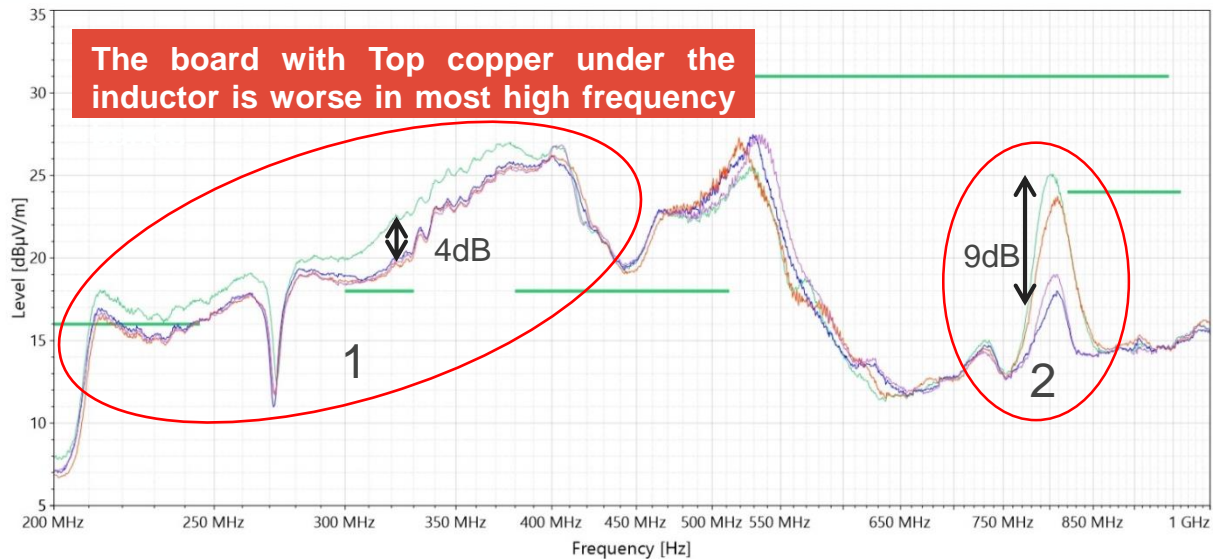
TB2: Removing Top copper

TB3: Removing Internal and Top copper

TB4: Removing all copper

Copper Under The Inductor: Test results

CISPR25 Class 5: RE Log Average measurements



The copper area under the inductor in top layer is Vout. The eddy currents are induced there. The Parasitic Capacitance between SW and Vout is increased by this extra area.

TB1: Copper under L

TB2: Removing Top copper

TB3: Removing Internal and Top copper

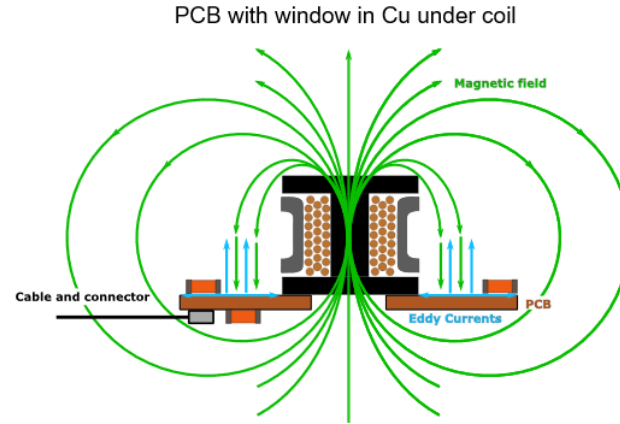
TB4: Removing all copper

Copper Under The Inductor: Conclusion

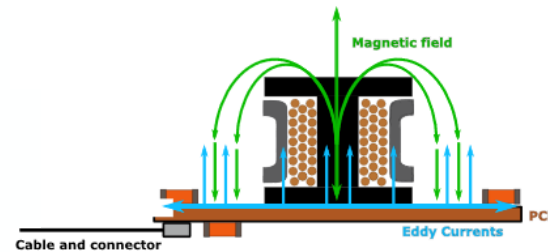
The magnetic fields emitted by the inductor create eddy currents when they hit perpendicular to a conductor.

These eddy currents create losses in the form of heat and reduce the effective inductance. However, the eddy currents also generate magnetic fields which oppose the inductor's one.

By placing copper under the inductor, most magnetic field is captured and converted to eddy currents so the emissions are lower.



PCB with no window in Cu under coil



Shielded & Semi-Shielded Inductor

Changed the standard molded inductor used in all other test MPL-AL4020-1R0 to the semi-shielded MPL-SE4030-1R0



APPLICATIONS

- Battery-powered devices
- Embedded computing
- High-current SMPS
- High-frequency SMPS
- POL converters
- FPGA

FEATURES

- Size 4.1mmx4.1mmx1.9mm
- Low DCR
- Low AC Losses
- Low Audible Noise
- Molded Construction
- Soft Saturation
- Stable Over High Temperatures
- Max Operating Temp +155°C
- RoHS/REACH-Compliant, Halogen-Free

ELECTRICAL CHARACTERISTICS

Parameter			Value	Unit
Inductance ⁽¹⁾	<i>L</i>	±20%	1.0	µH
Resistance	<i>R_{DC}</i>	typ	10.1	mΩ
Resistance _{MAX}	<i>R_{DC MAX}</i>	max	11.8	mΩ
Rated Current ⁽²⁾	<i>I_R</i>	typ	7.9	A
Saturation Current _{25°C} ⁽³⁾	<i>I_{SAT 25°C}</i>	typ	8.6	A
Saturation Current _{100°C} ⁽⁴⁾	<i>I_{SAT 100°C}</i>	typ	8.6	A
Resonance Frequency	<i>f_r</i>	typ	56	MHz

$$C_p=8pF$$



APPLICATIONS

- Battery-powered devices
- High-efficiency SMPS
- Embedded computing
- Input filters

FEATURES

- Size 4mmx4mmx3mm
- Semi-Shielded Construction
- Low DCR
- Low Stray Field
- Max Operating Temp +125°C
- RoHS/REACH-Compliant, Halogen-Free

ELECTRICAL CHARACTERISTICS

Parameter			Value	Unit
Inductance ⁽¹⁾	<i>L</i>	±20%	1.0	µH
Resistance	<i>R_{DC}</i>	typ	12.5	mΩ
Resistance _{MAX}	<i>R_{DC MAX}</i>	max	15	mΩ
Rated Current ⁽²⁾	<i>I_R</i>	typ	6.3	A
Saturation Current _{25°C} ⁽³⁾	<i>I_{SAT 25°C}</i>	typ	7.5	A
Saturation Current _{100°C} ⁽⁴⁾	<i>I_{SAT 100°C}</i>	typ	7.2	A
Resonance Frequency	<i>f_r</i>	typ	90	MHz

$$C_p=3pF$$

Shielded & Semi-Shielded Inductor: Test Results

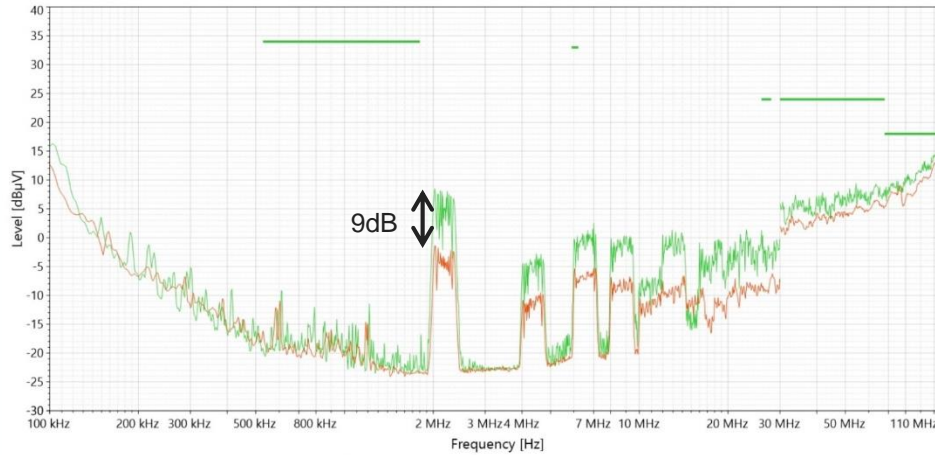
Molded Inductor



Semi-Shielded Inductor

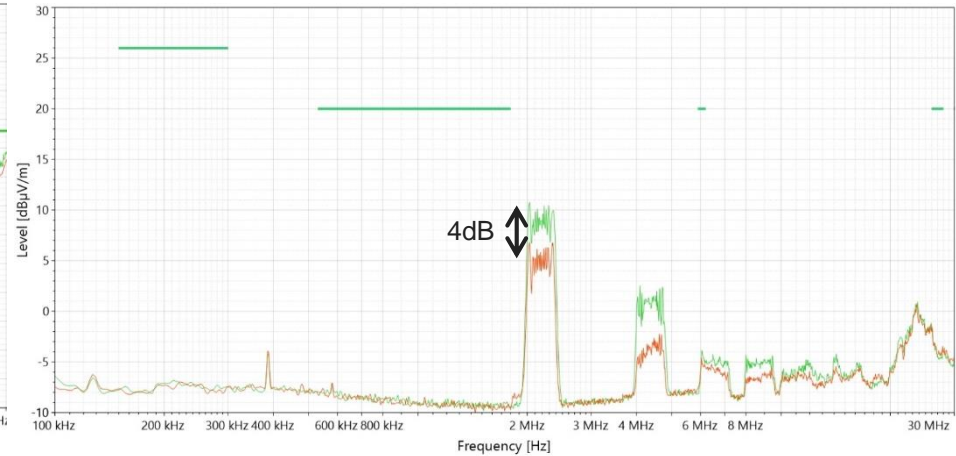


CISPR25 Class 5: CE Average measurements



The semi-shielded inductor is much better at low frequency and helps at the FM band.

CISPR25 Class 5: Monopole Average measurements



The semi-shielded inductor emits less E-field.

Shielded & Semi-Shielded Inductor: Test Results

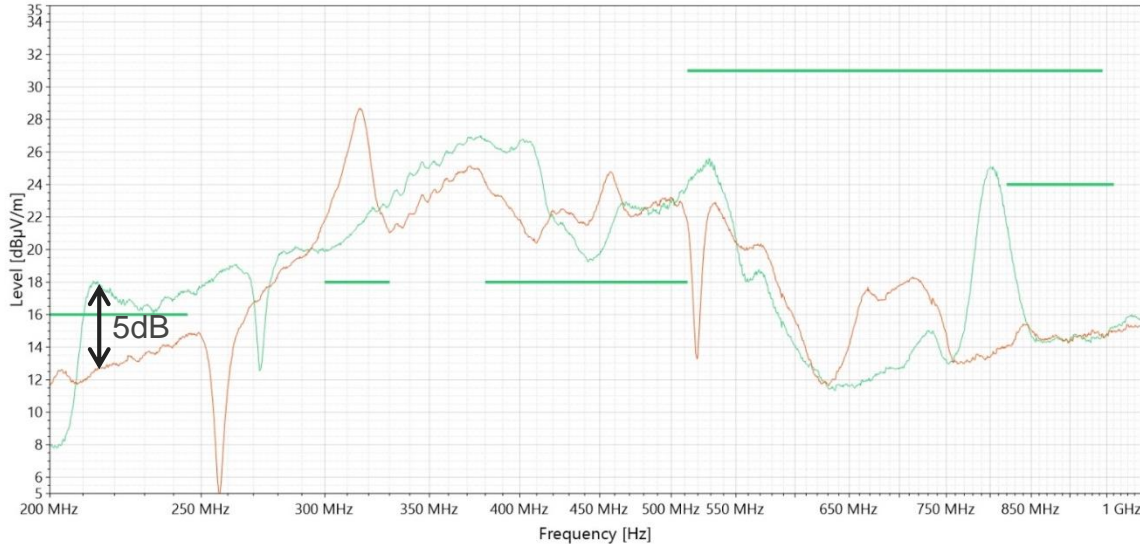
Molded Inductor



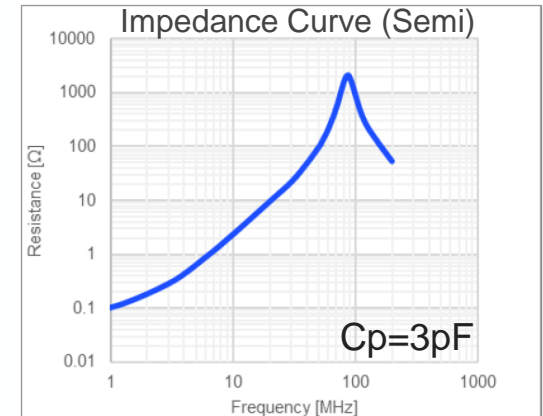
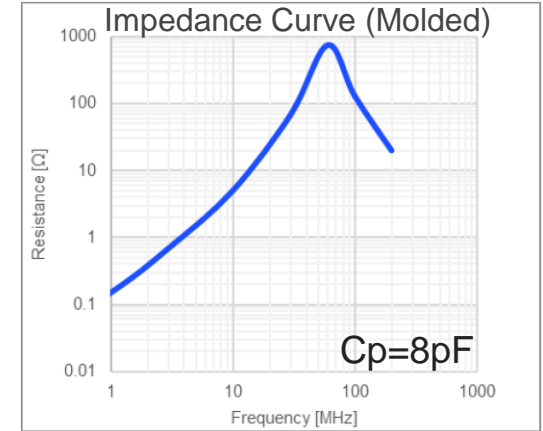
Semi-Shielded Inductor



CISPR25 Class 5: RE Log Average measurements (vertical)

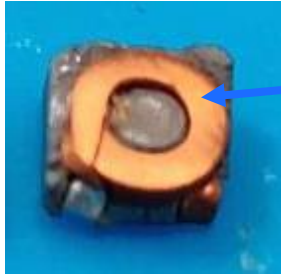


Overall the semi-shielded looks better except for the resonance at 320MHz.

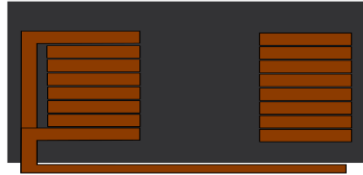


Shielded Inductor: Conclusion

Shielded inductors are not always having better EMI performance compared to non-shielded or *semi-shielded inductors*. Each design is unique, you have to test in the early stages and evaluate which components are best. Not all inductors are built equal.



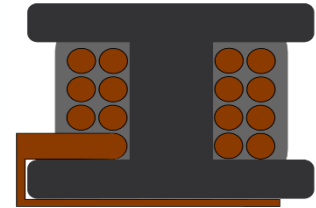
Larger area for E-field radiation



Shielded (molded)

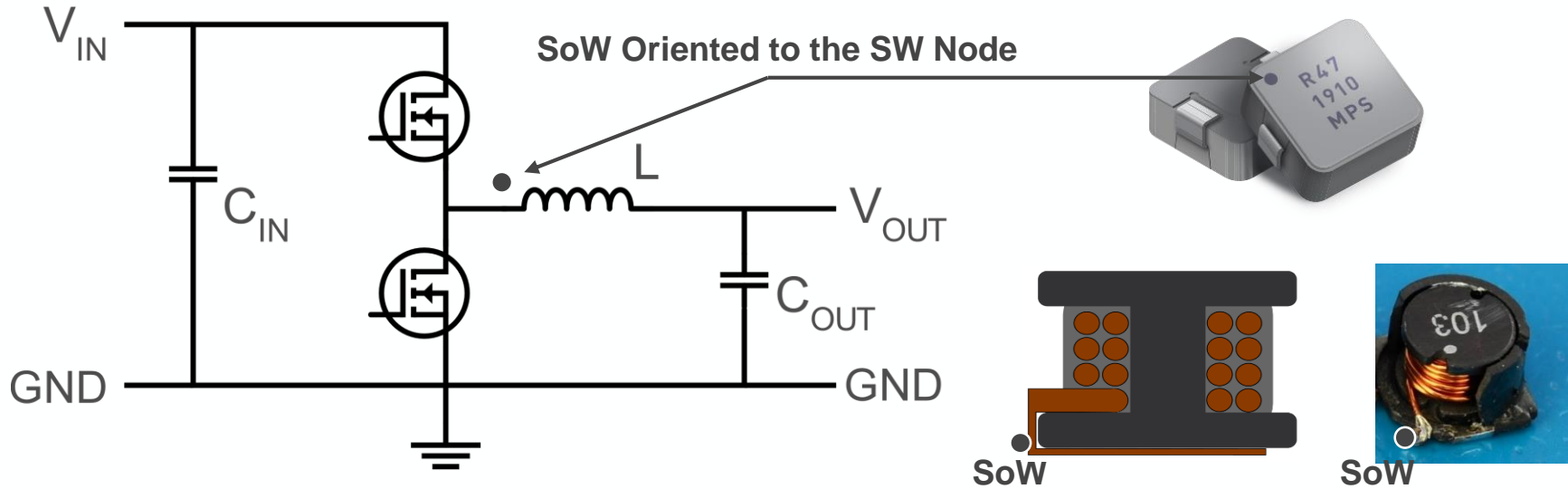


Semi-Shielded (epoxy coating)



Orientation of Inductor (Start of Winding)

The converter switch node is close to the start of winding (SoW) side.

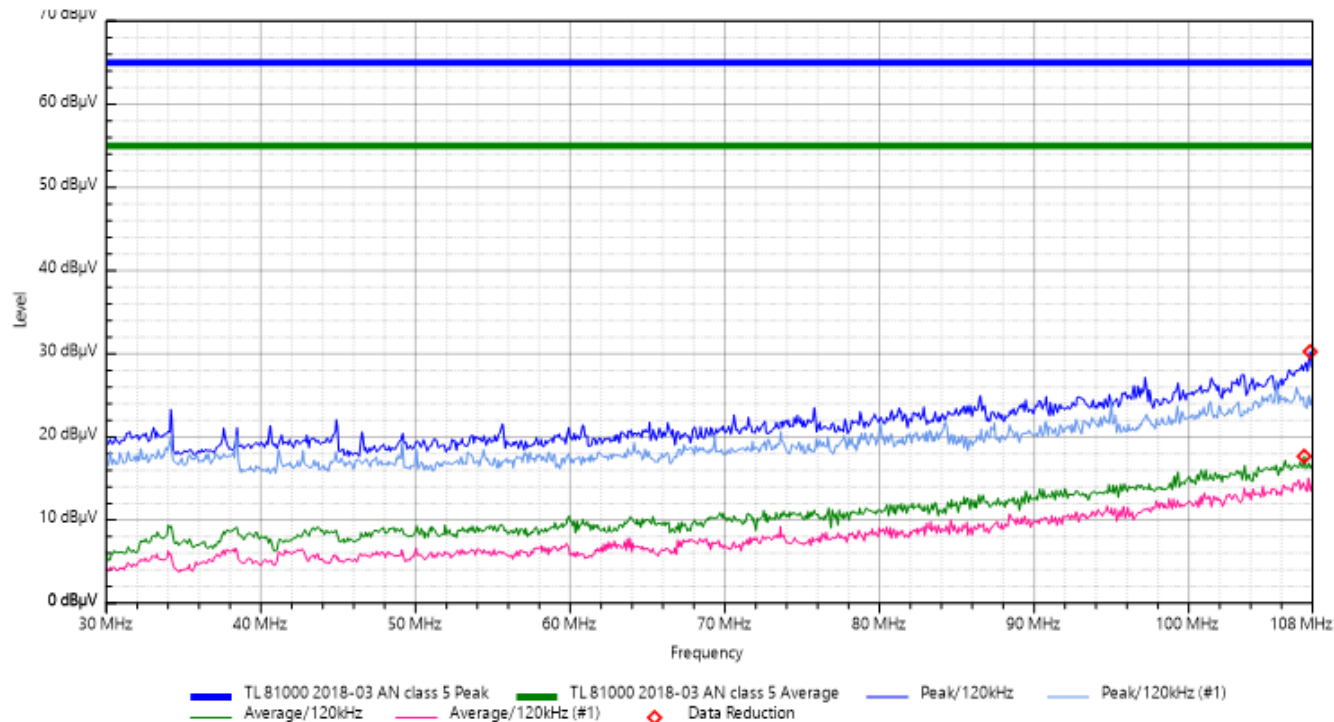


- Avoids audible noise from harmonics
- Reduces emissions caused by the inductor

Orientation of Inductor - XAL5030 1 μ H in Both Directions

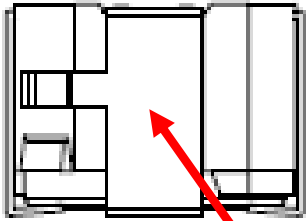
Start of Winding at SW is 2-3dB better

B3

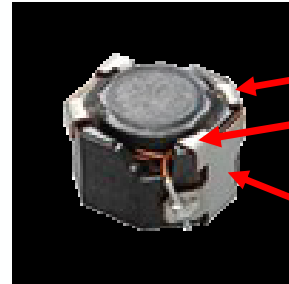


Orientation of Inductor (Start of Winding)

4.5mm Height



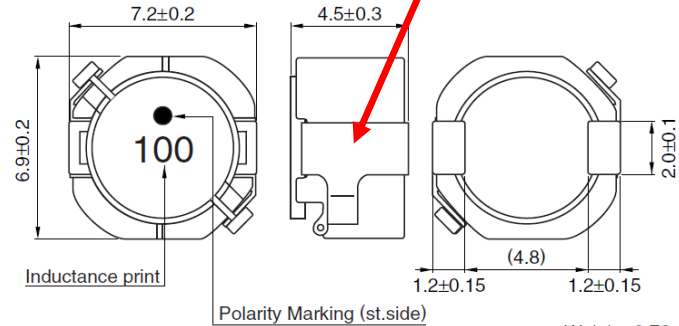
Contact metal acts as antenna for E-field from SW-node dV/dt



End of Winding side
Contact metal with two clip into airgap for mechanical robustness

Even if SoW is at SW, plate will cause trouble

SHAPES AND DIMENSIONS

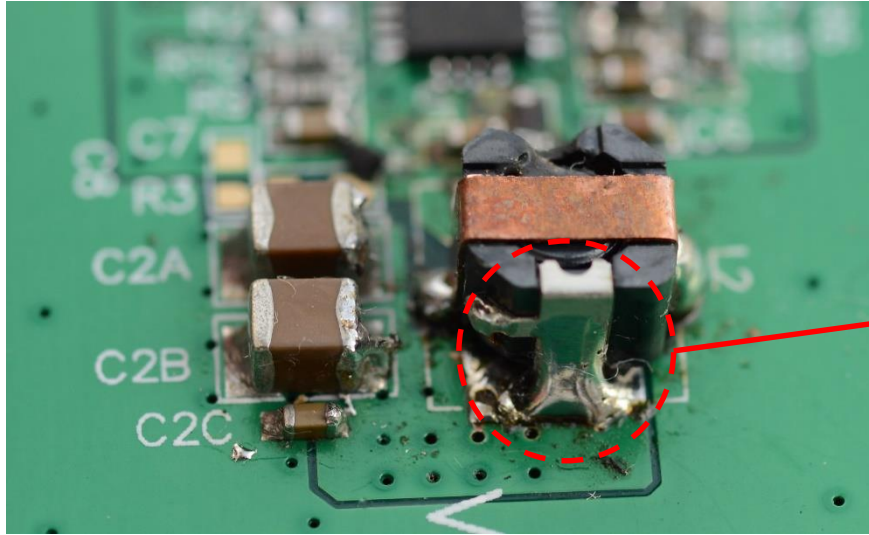


Weight: 0.72g

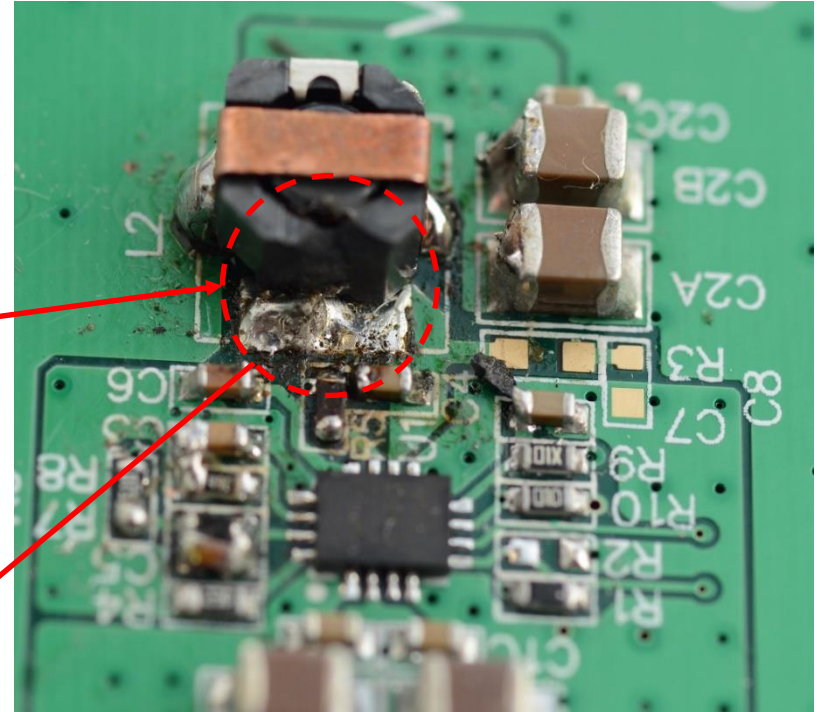
Dimensions in mm

Example Drawings from Murata, TDK and ABC

Orientation of Inductor (Start of Winding)

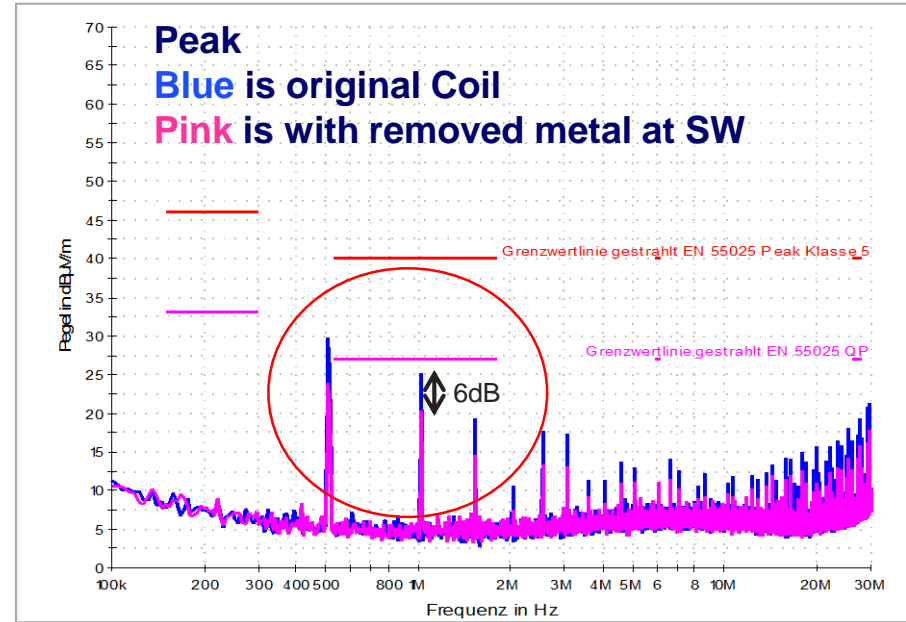
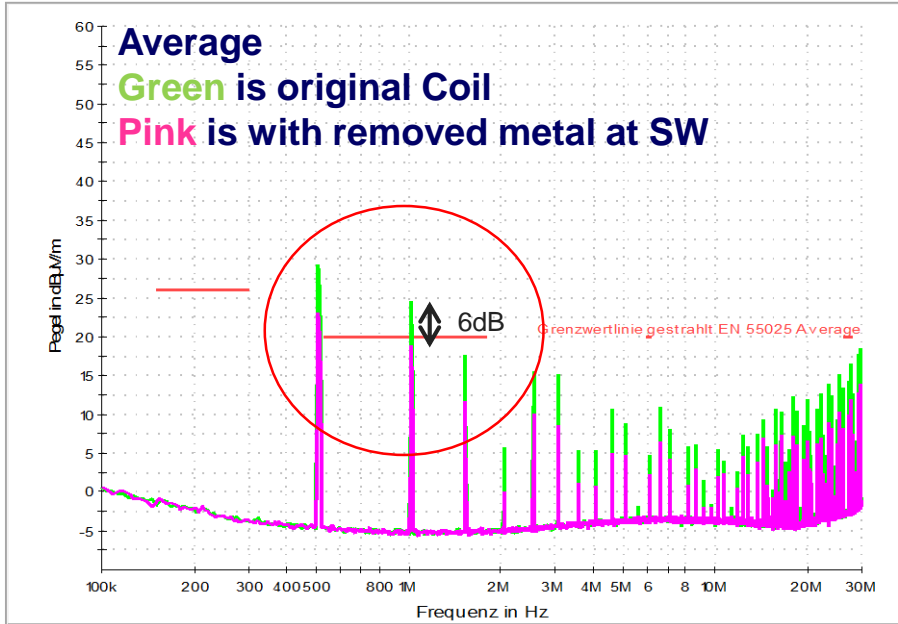


SW-node contact plate removed:



4.5mm height contact plate act as E-Field antenna for SW-node high dV/dt .
Optimum coil should have SW-contact at the bottom.

Orientation of Inductor (Start of Winding)



SW-node contact plate removed:
Winding soldered directly to PCB.
6 dB lower emissions at 1MHz
In Monopole Antenna Test

Conclusions

- **Inductor**

- An Inductor Reacts to Current Changes
- Stores Induced Electric Energy as Magnetic Energy
- Inductance Depends on the Core Material Characteristics and Number of Turns
- Rated Current & Saturation Current
- SoW Orientation.

- **Inductance Selection**

- Topology Determined.
- Design Target: Current Ripple, Voltage Ripple.
- Worst Case Working Condition: Input Voltage Range, OCP & SCP.

- **Influence of EMI**

- Copper Under Inductor.
- Shielded Inductor / Inductor Structure – Smaller Size Preferred.
- Place SoW At DCDC SW Terminal.

The screenshot displays the MPS website interface. At the top, there is a navigation menu with links for '产品' (Products), '应用' (Applications), '设计' (Design), '支持' (Support), '订购' (Ordering), 'EMC实验室' (EMC Lab), '关于MPS' (About MPS), and '联系方式' (Contact Us). On the right side of the header, there are links for '我的购物车' (My Cart), '中文' (Chinese), '登录' (Login), and '注册' (Register). A search bar is located below the navigation menu.

The main content area features two large promotional banners:

- 高隔离应用电流传感器** (High Isolation Application Current Sensor): Includes a video player icon and a '观看视频' (Watch Video) button.
- 新品速递 — MA600 替代昂贵的光编码器 高精度数字化磁性角度传感器** (New Product Delivery — MA600 Replaces Expensive Optical Encoders, High-Precision Digital Magnetic Angle Sensor): Includes an image of a robotic arm and a '了解更多' (Learn More) button.

Below the banners are four product category tiles:

- 集成电感的电源模块** (Integrated Inductor Power Module): Features an image of a power module and a '查看模块' (View Module) button. Text includes '可配置、降压、升压、USB、PDE' and '3A 15A'.
- 磁性位置 & 电流传感器** (Magnetic Position & Current Sensor): Features an image of a sensor and a '查看传感器' (View Sensor) button.
- 单片IC** (Single-Chip IC): Features an image of an IC and a '查看单片IC' (View Single-Chip IC) button. Text includes 'DC/DC, BMS, LED, 电烙丝、传感器'.
- AC/DC 功率转换** (AC/DC Power Conversion): Features an image of a power converter and a 'AC/DC 产品' (AC/DC Products) button. Text includes '反激控制器, LED, 整流器, LLC 设计工具'.

更多电源/电感解决方案，欢迎访问：<https://www.monolithicpower.cn>