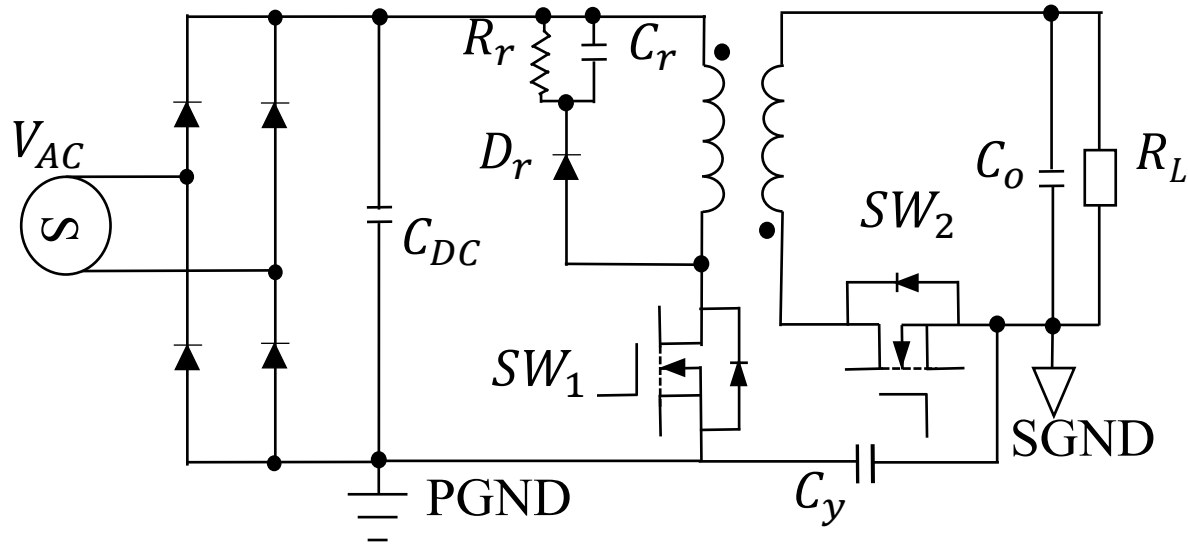

Analysis and Suppression of Conductive and Radiated Electromagnetic Interference for Flyback Converters

(Aug. 21th, 2025)

Shuo Wang, University of Florida
Gainesville, FL 32611

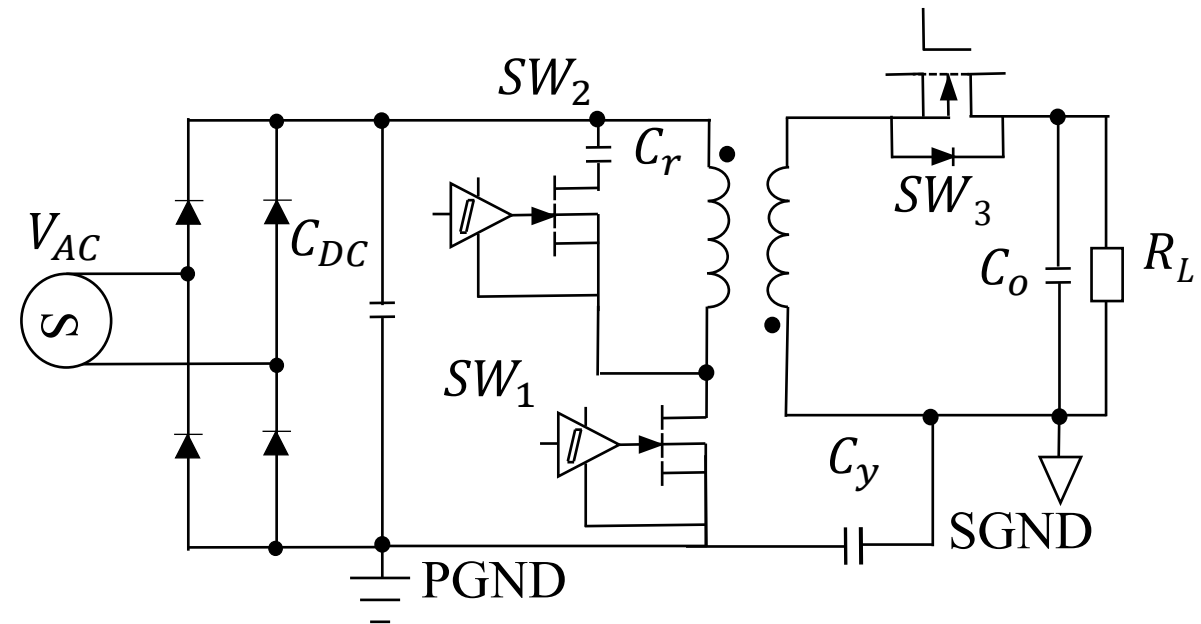
Note: Please cite our work/papers when you publish or share the related work, it is very important to us as it means respect to our contributions

Popular Flyback Converter Topologies



**Flyback Converter with
Synchronous Rectifiers / Diodes**

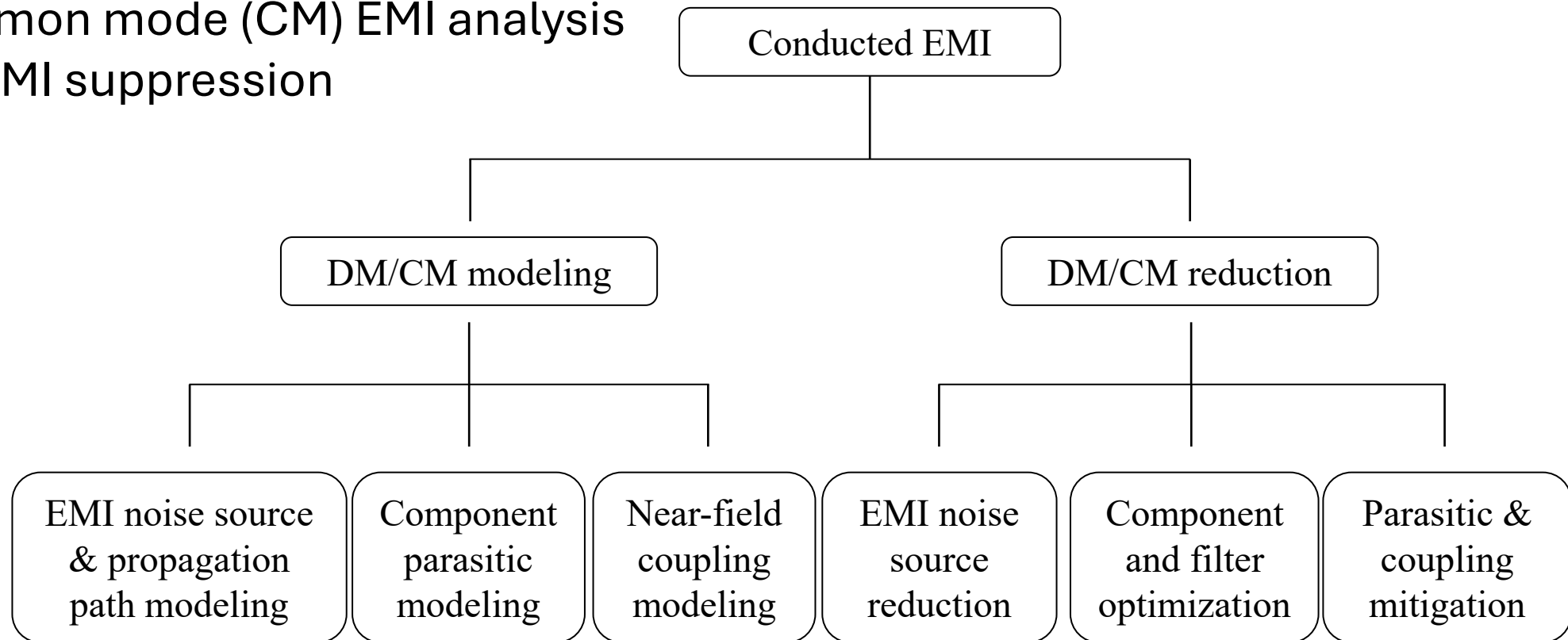
**Active Clamped Flyback Converter
with Synchronous Rectifiers / Diodes**



Conductive EMI

Conductive EMI:

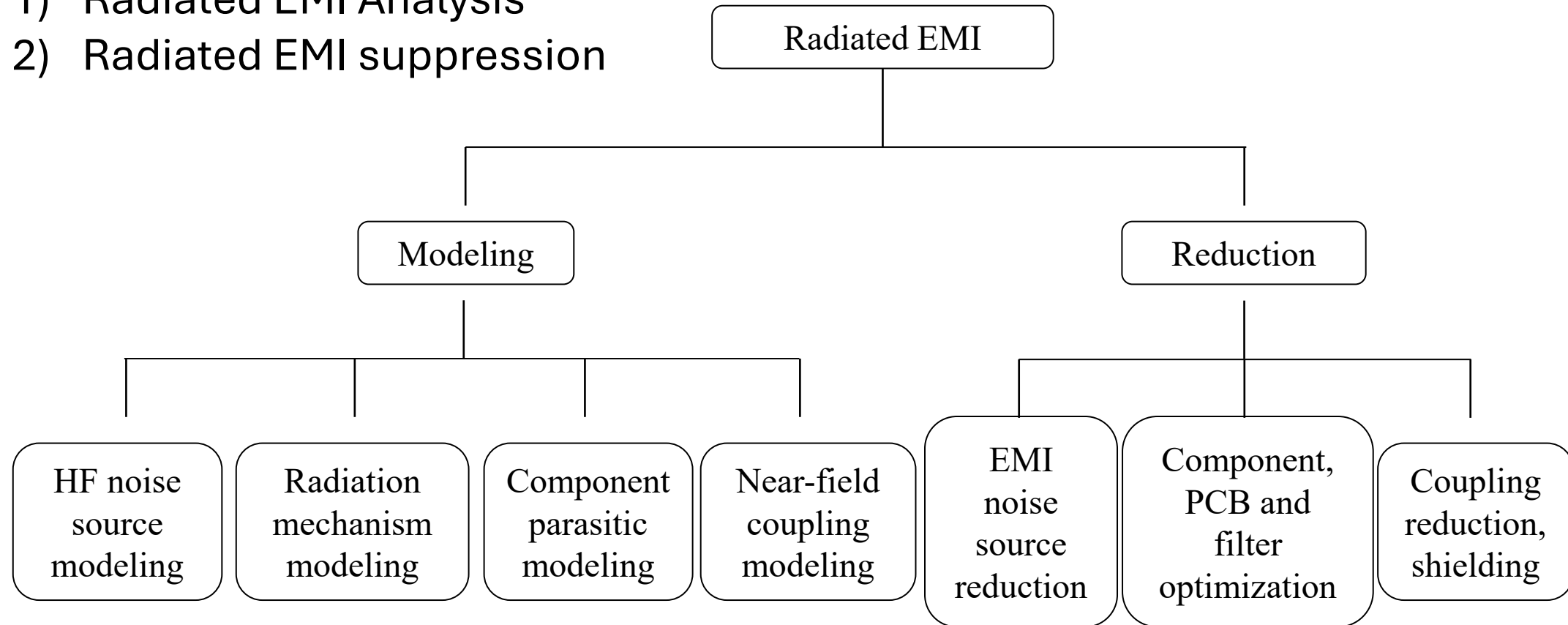
- 1) Differential Mode (DM) EMI analysis
- 2) DM EMI suppression
- 3) Common mode (CM) EMI analysis
- 4) CM EMI suppression



Radiated EMI

Radiated EMI:

- 1) Radiated EMI Analysis
- 2) Radiated EMI suppression

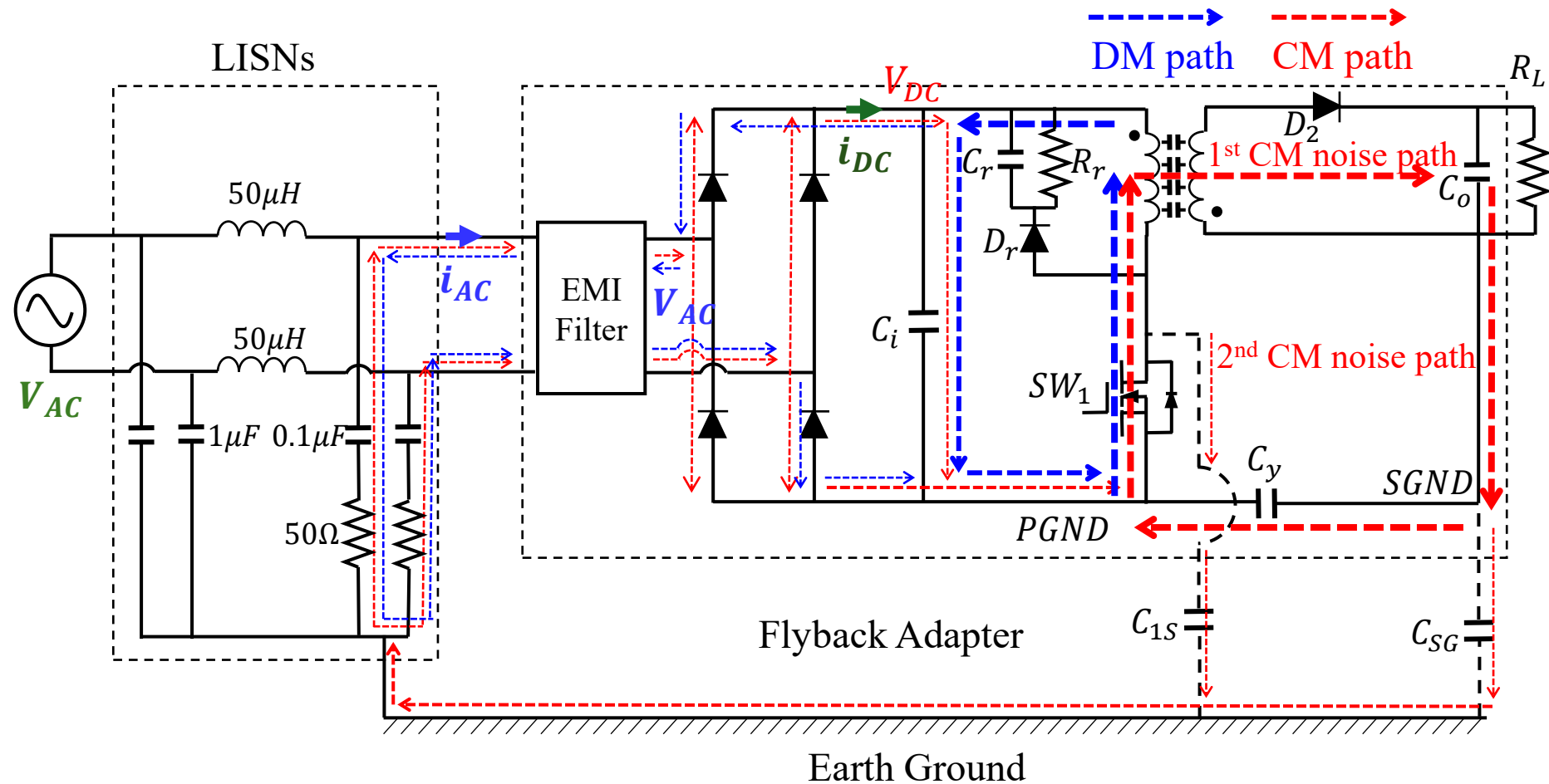
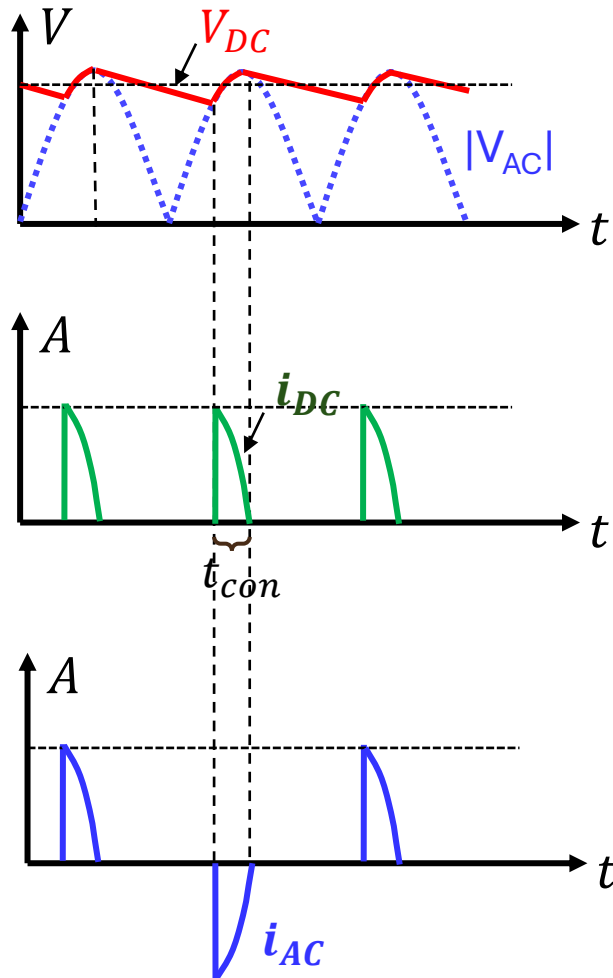


AC-line DM EMI Filters vs DC-bus DM EMI Filters

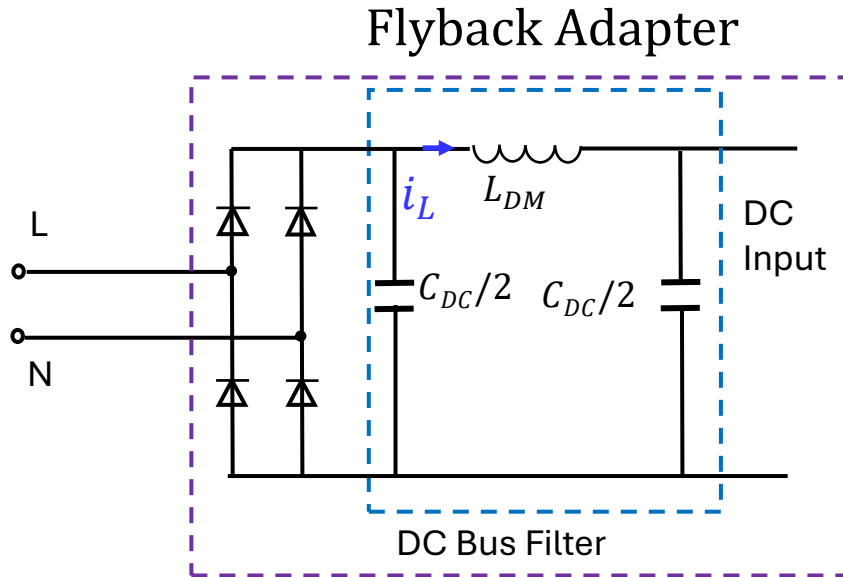
[1] Y. Li, L. Yang, S. Wang, H. Sheng, S. Lakshmikanthan, and L. Jia, "Investigation of a DC bus differential mode EMI filter for AC/DC power adapters," in *2018 IEEE Applied Power Electronics Conference and Exposition (APEC)*, 2018, pp. 603-610.

DM EMI, CM EMI and Line-frequency Currents of Flyback Converters

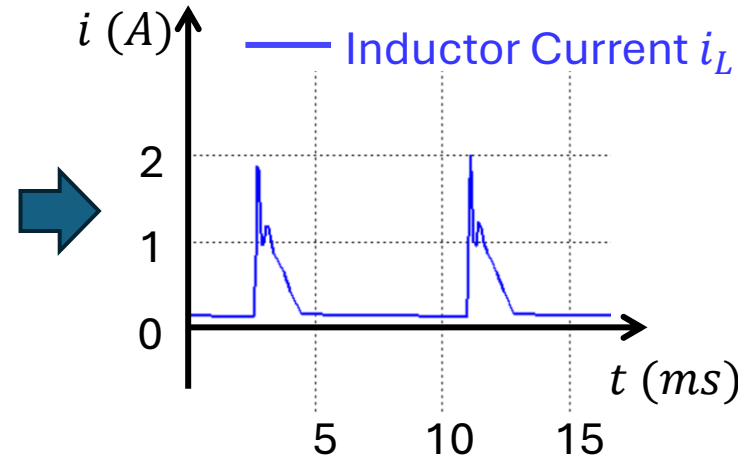
line-frequency power current



Flyback Converter's DM EMI Filter Selection based on Line-frequency Currents



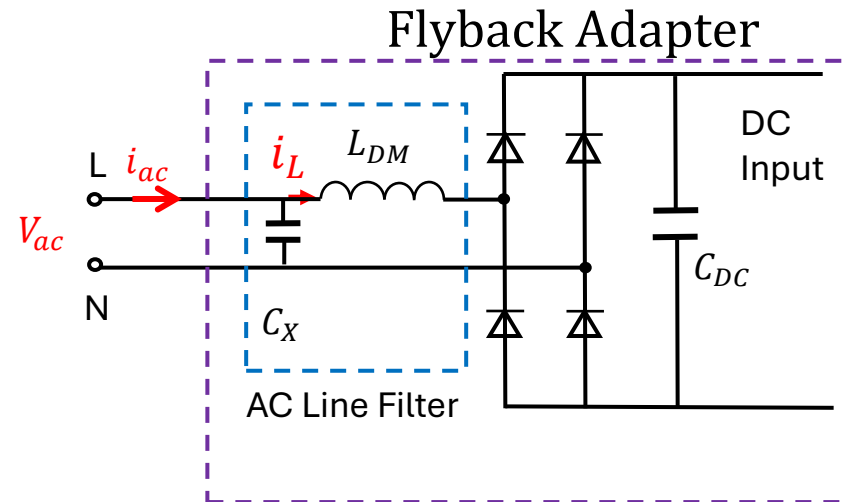
DC-bus filter topology



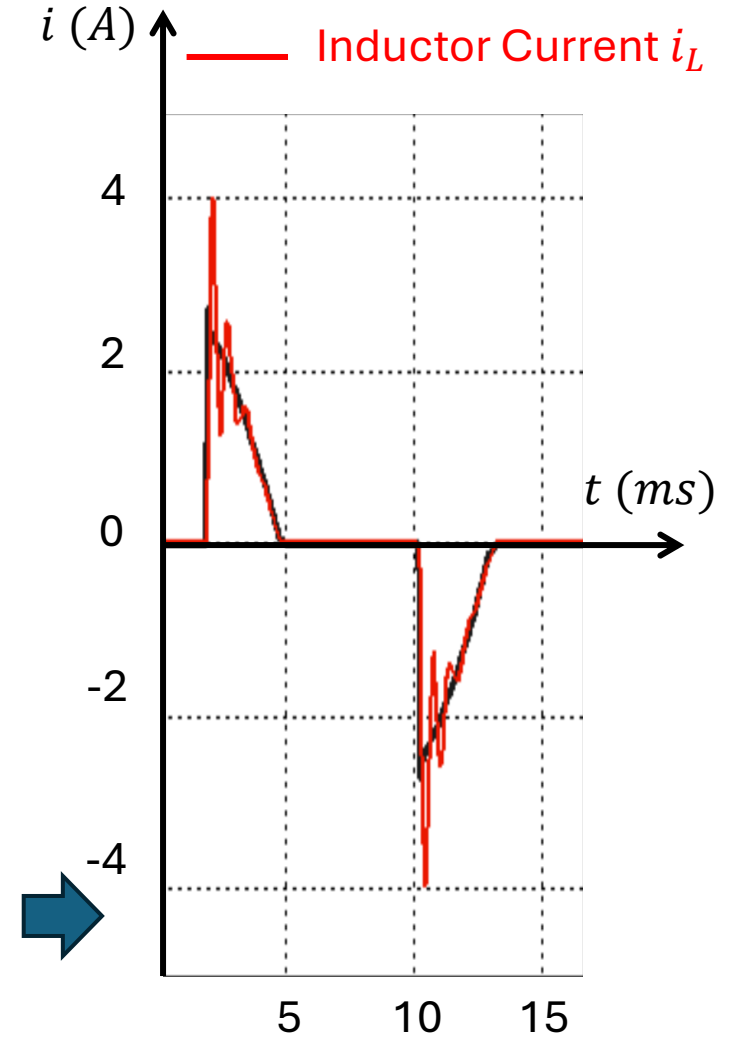
C1 absorbs part of peak currents

Conclusion:

An AC-line EMI filter has much higher inductor current peaks than a DC bus filter



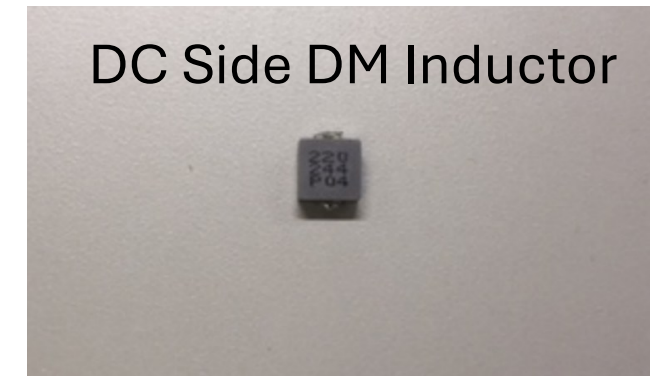
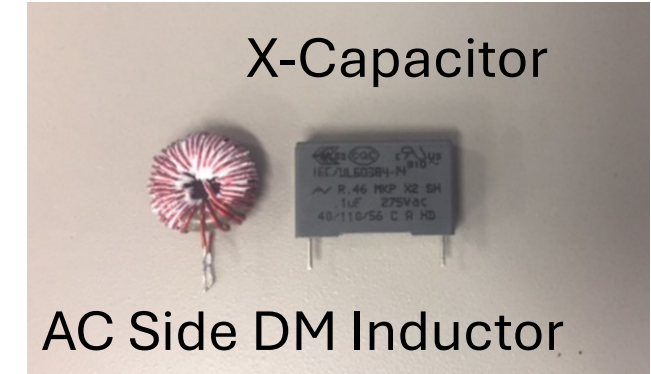
AC line filter topology



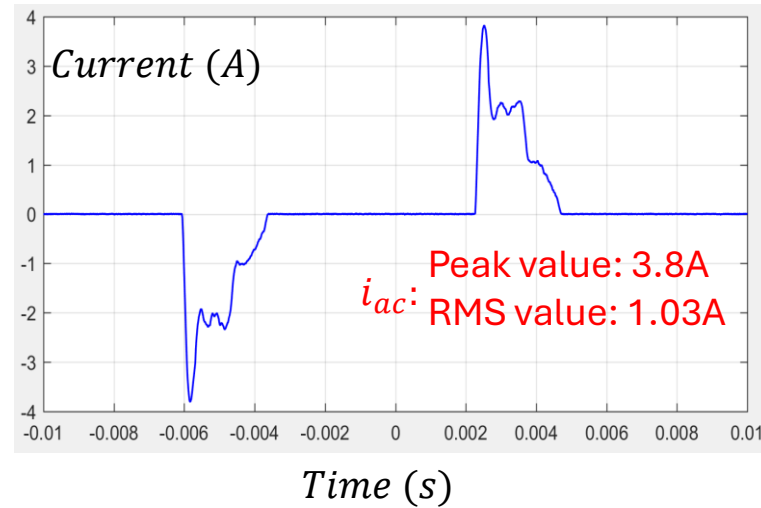
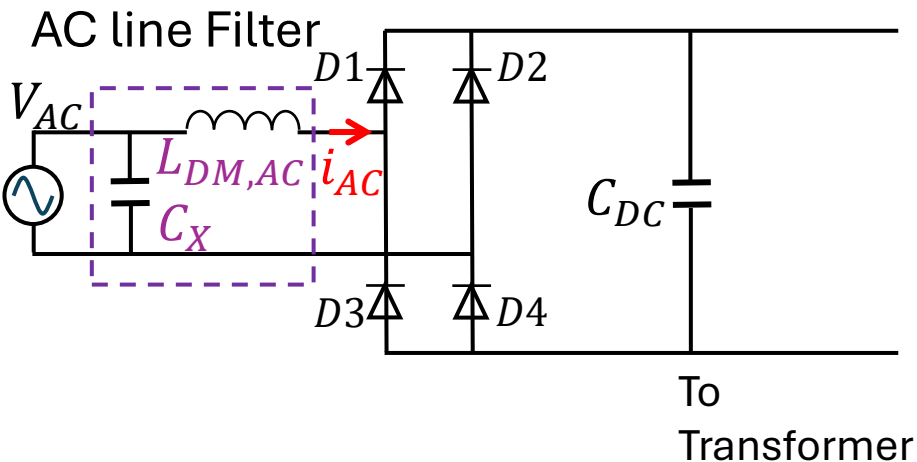
DC-bus DM EMI Filter Size vs AC-line DM EMI Filter Size

Component	AC Line Filter			DC Bus Filter		
	Value	PCB Size (mm^2)	Volume (mm^3)	Value	PCB Size (mm^2)	Volume (mm^3)
DC Capacitor	$68\mu F$	320	4000	$2 * 33\mu F$	312	4410
X Capacitor	$0.1\mu F$	90	850	N/A	N/A	N/A
DM Inductor	$100\mu H$	72	860	$22\mu H$	50	350
Total		482	5710		362	4760

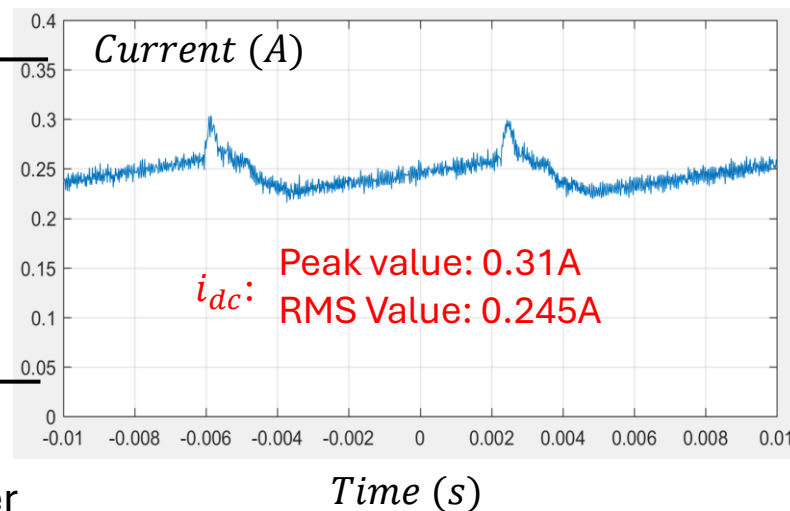
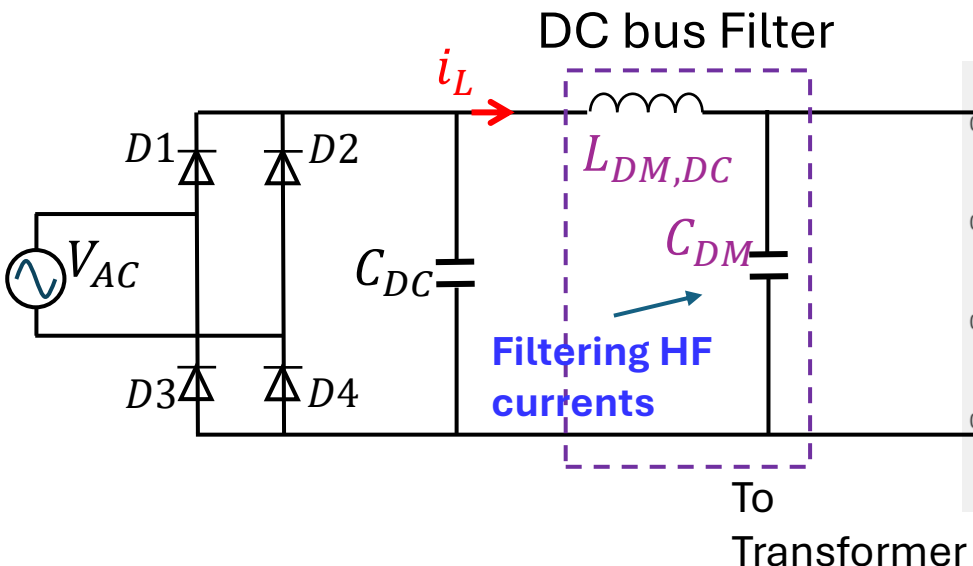
Conclusion: The size of a DC bus filter in a flyback converter is much smaller than that of an AC line filter.



Further Improving DC-bus DM EMI Filter Design



AC Line Filter	Size (mm ²)	Volume (mm ³)
0.47uF/275VAC Film X Capacitor	180	2898
300uH Inductor, High Flux Core	148	2133
Total	328	5031



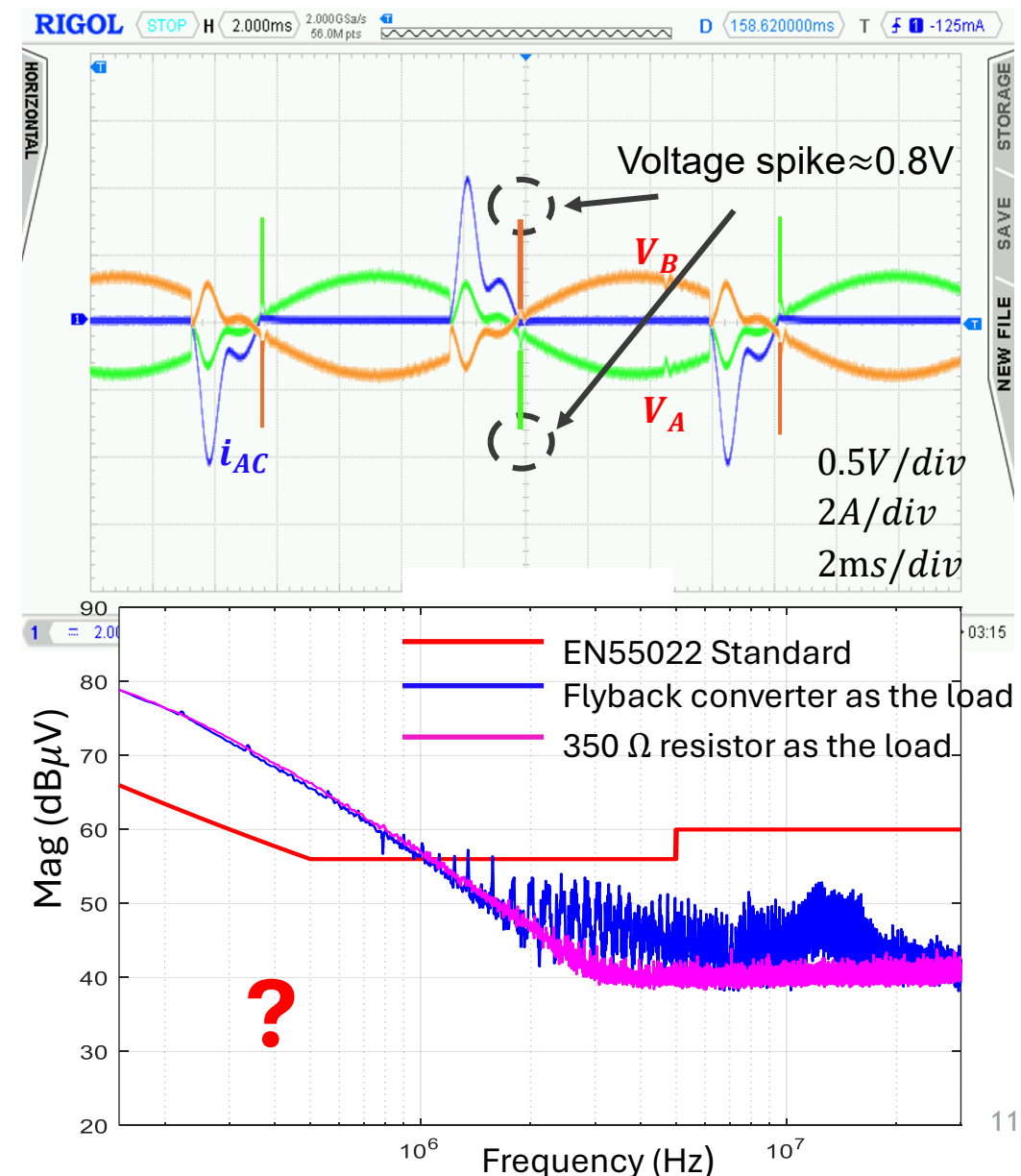
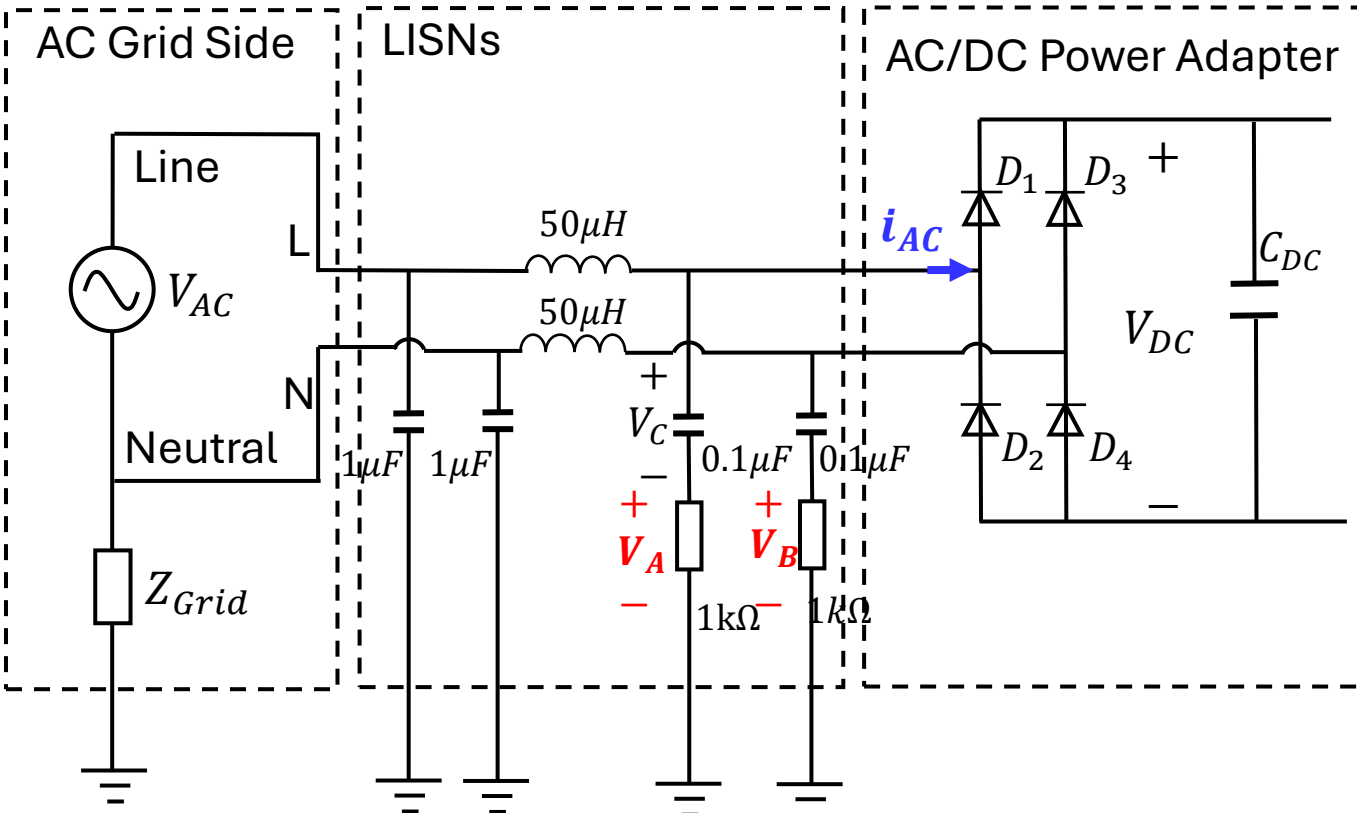
DC bus Filter	Size (mm ²)	Volume (mm ³)
1.0uF/630VDC X7R DM Capacitor	30	165
300uH Inductor, MPP Core	52	327
Total	82	492

Conclusion: Both the volume and cost of DC filters are much lower than those of AC filters.

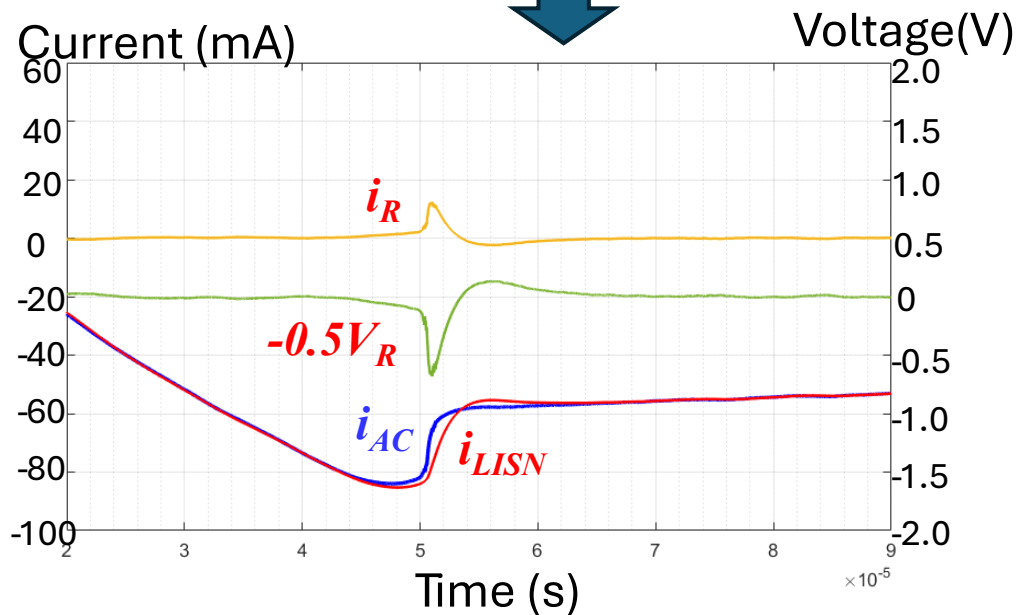
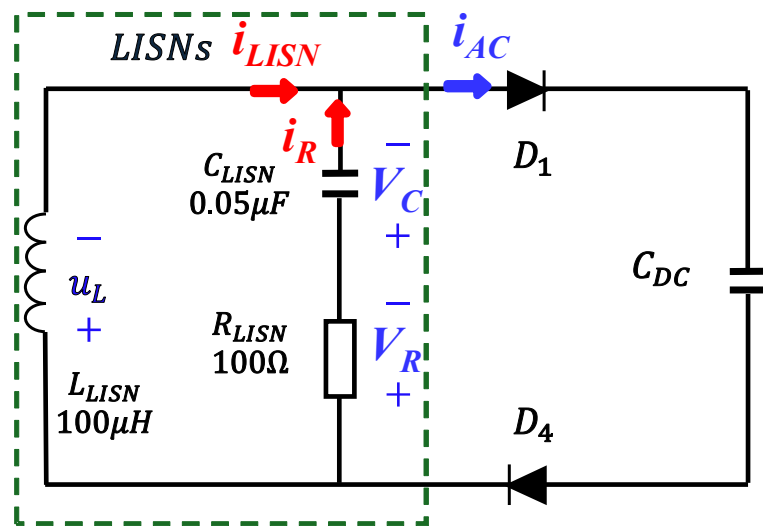
DM EMI Noise due to Diode Bridge Reverse Recovery

[2] Z. Ma, Y. Li, S. Wang, H. Sheng, and S. Lakshmikanthan, "Investigation and Reduction of EMI Noise Due to the Reverse Recovery Currents of 50/60 Hz Diode Rectifiers," *IEEE Journal of Emerging and Selected Topics in Industrial Electronics*, vol. 3, no. 3, pp. 594-603, 2022.

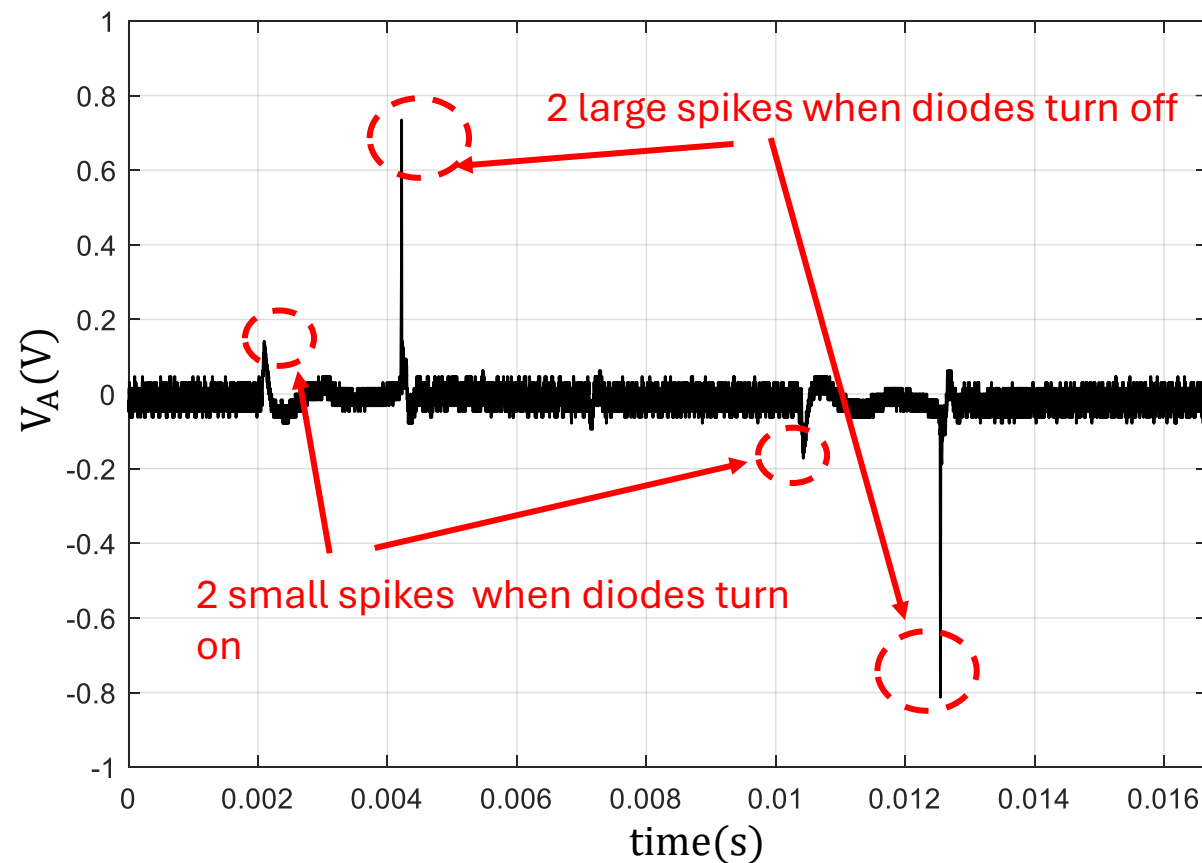
High DM EMI Noise with a 50/60Hz diode Bridge



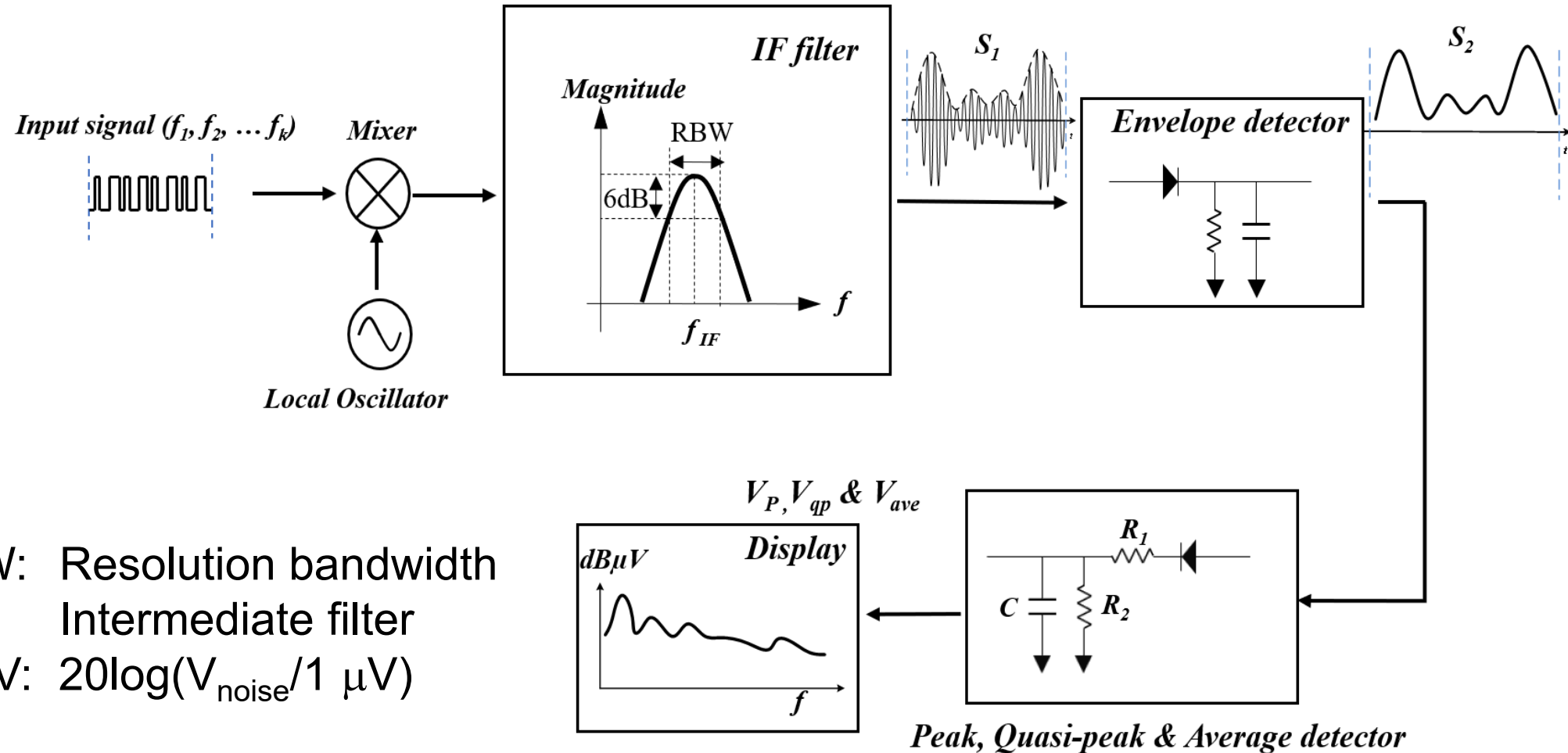
Voltage Spikes on LISNs due to Diode Reverse Recovery



Measured spikes in time-domain at the output of a DM Noise Separator

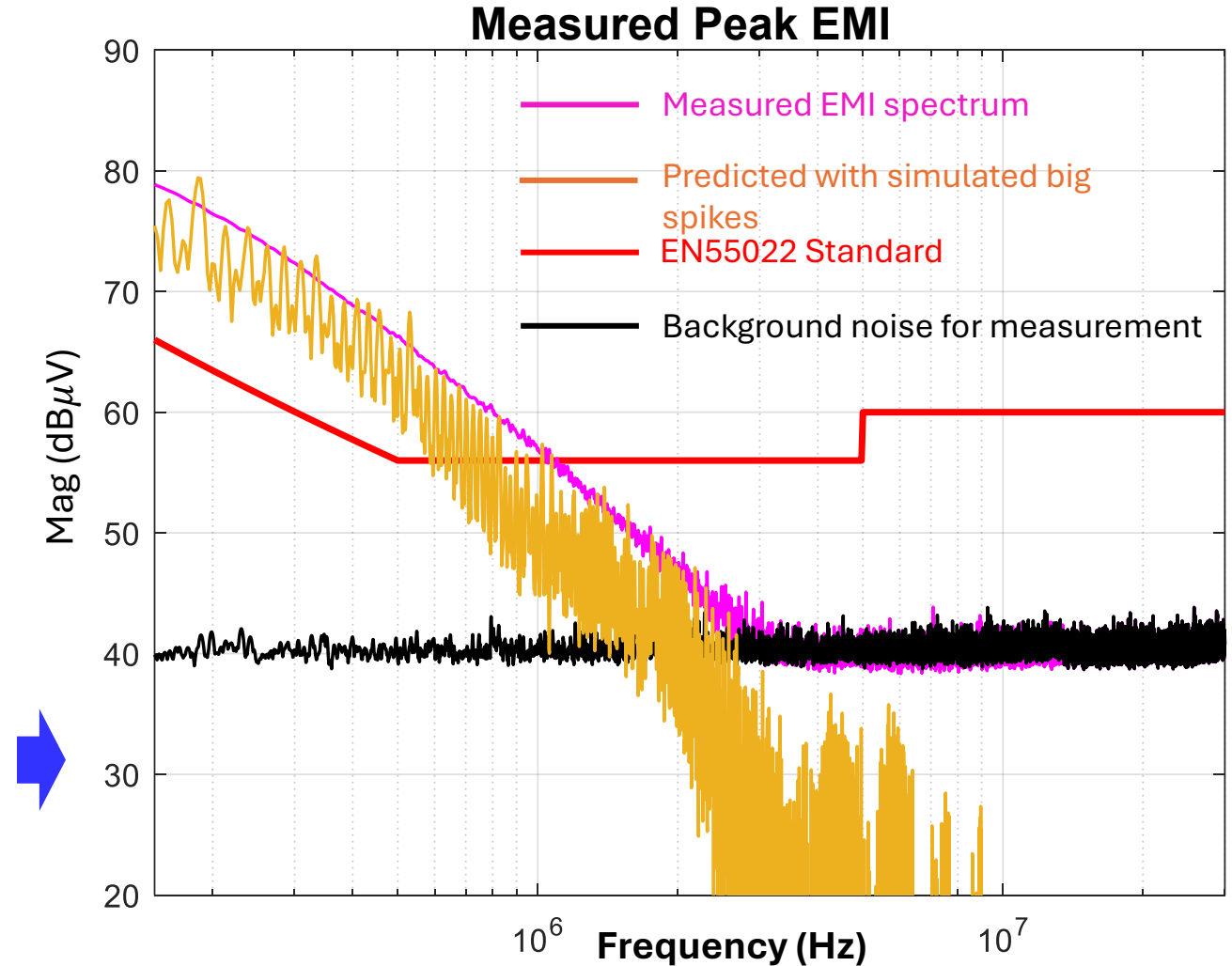
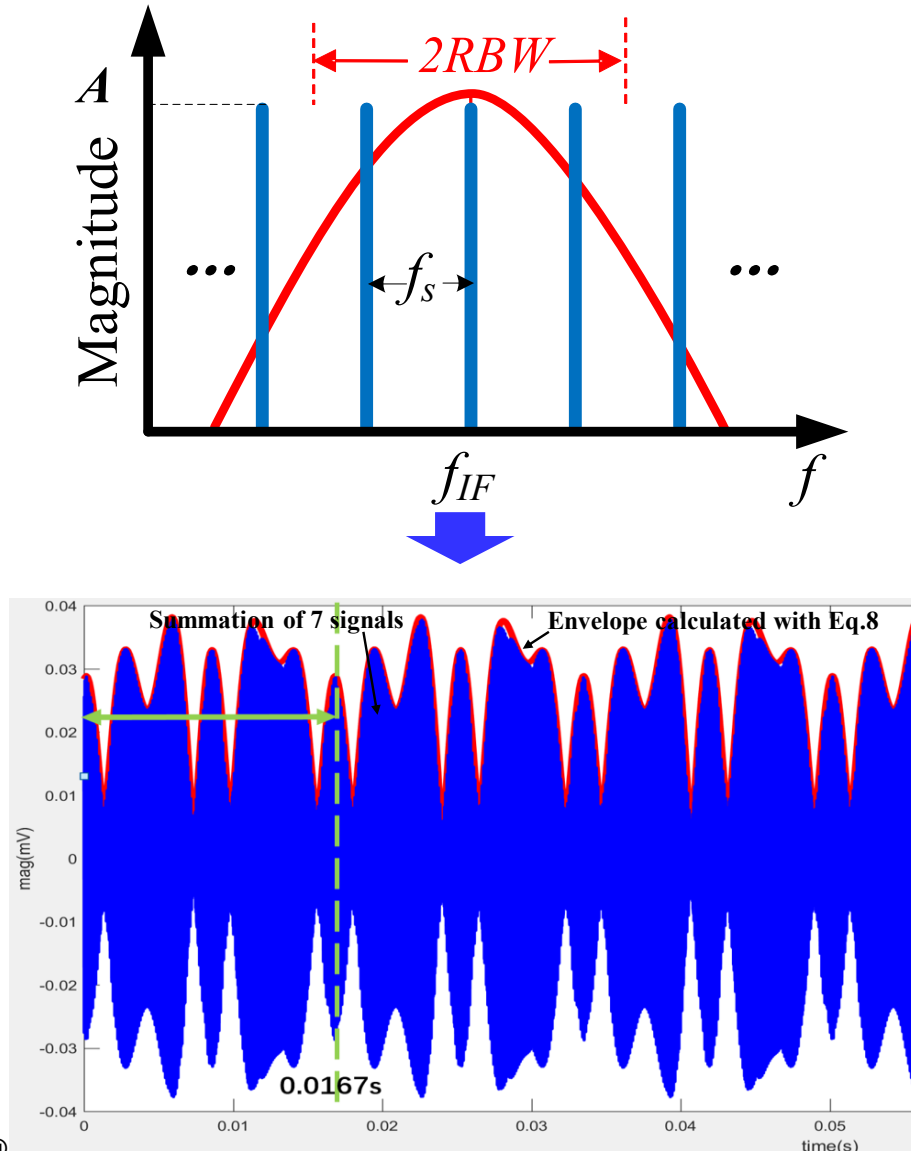


Operating Principle of A Spectrum Analyzer



RBW: Resolution bandwidth
 IF: Intermediate filter
 dBμV: $20\log(V_{\text{noise}}/1 \mu\text{V})$

Many Orders of 50/60Hz Harmonics Contribute to Measured High DM EMI at a Single Frequency



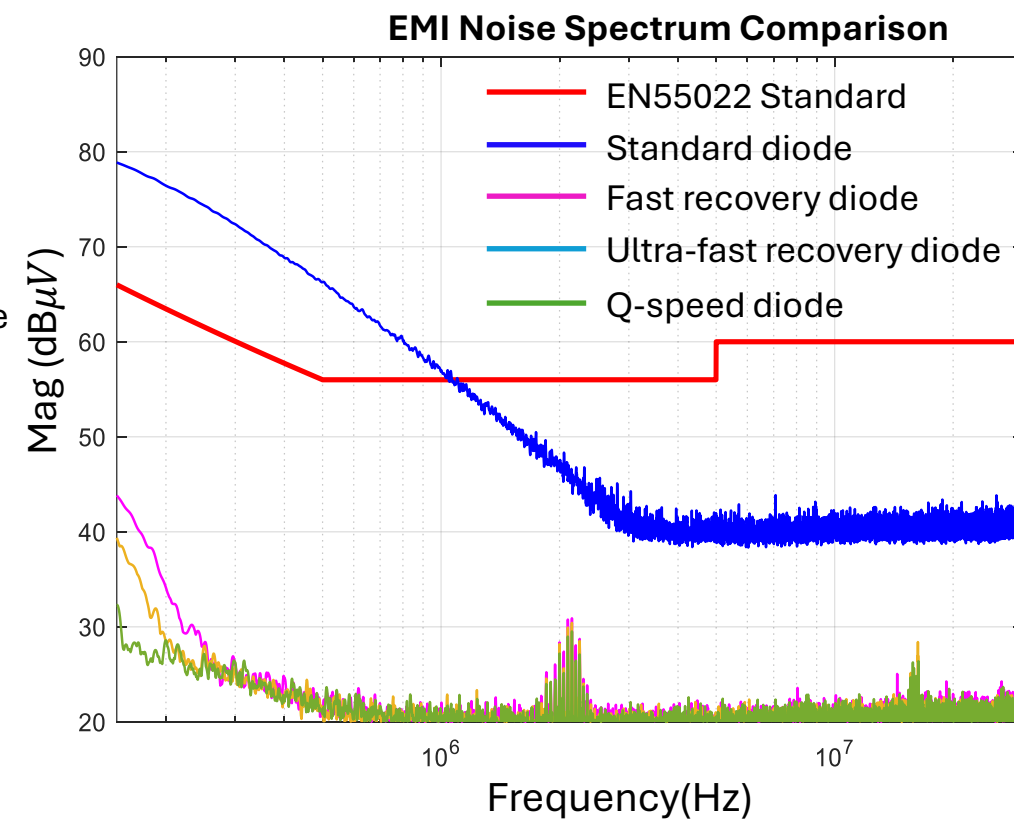
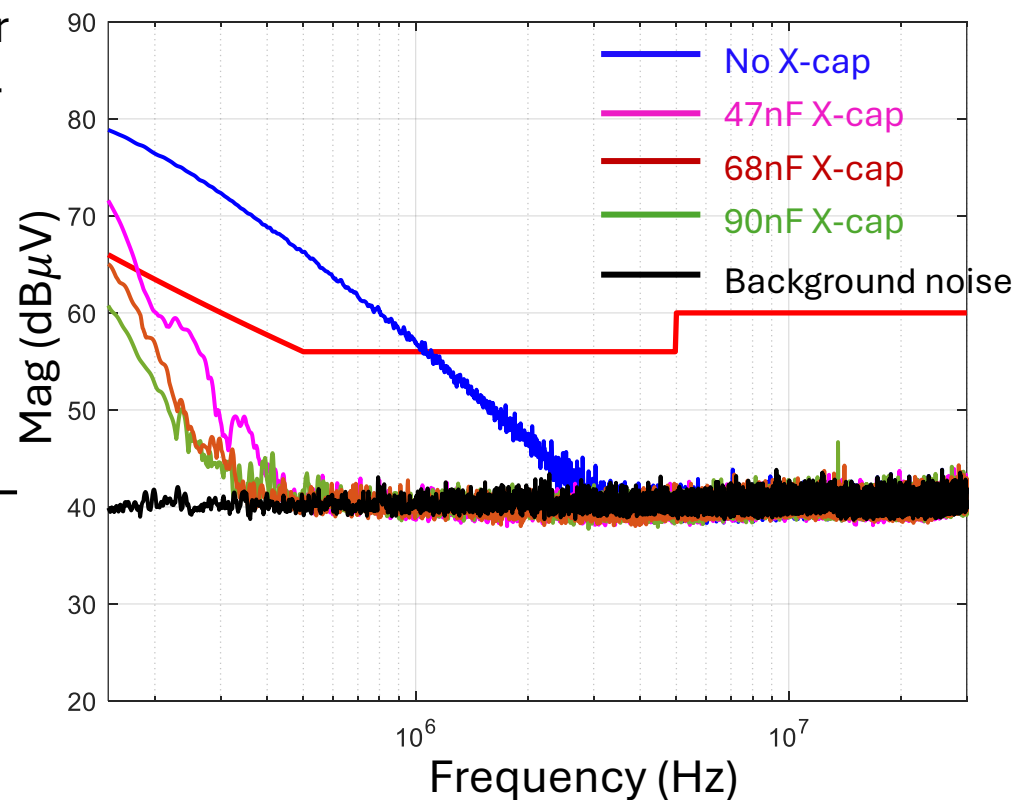
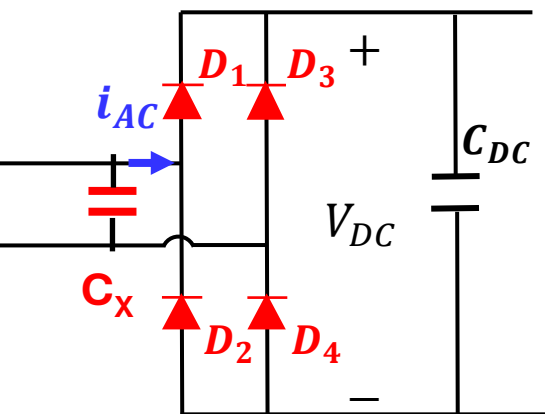
[3]: L. Yang, S. Wang, H. Zhao and Y. Zhi, "Prediction and Analysis of EMI Spectrum Based on the Operating Principle of EMC Spectrum Analyzers," in *IEEE Transactions on Power Electronics*, vol. 35, no. 1, pp. 263-275, Jan. 2020, doi: 10.1109/TPEL.2019.2914468.

DM EMI Suppression Solutions

- 1) Add a X-cap: C_x to filter out HF harmonics
- 2) Use fast recovery rectifier diodes to eliminate the effects of reverse recovery currents



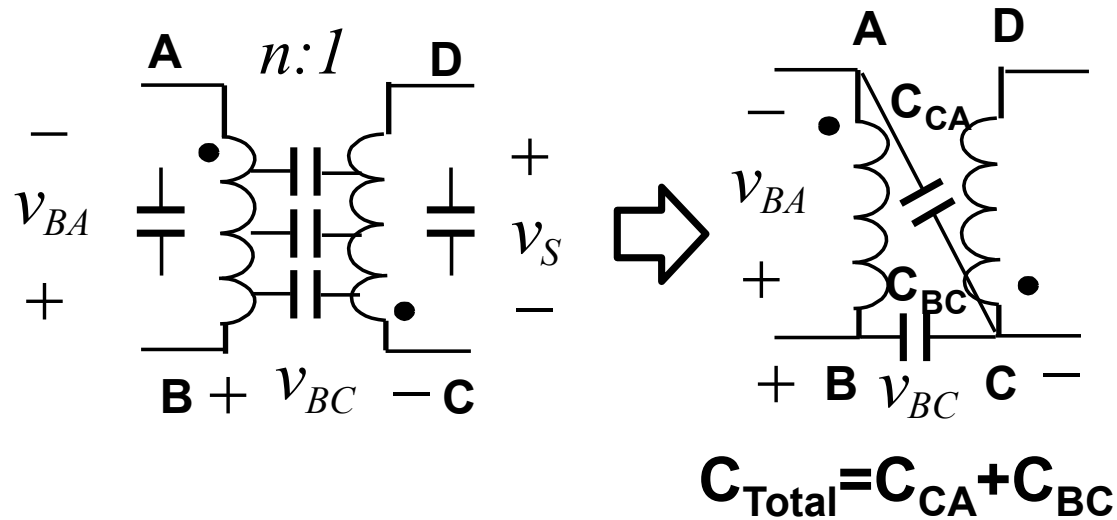
AC/DC Power Adapter



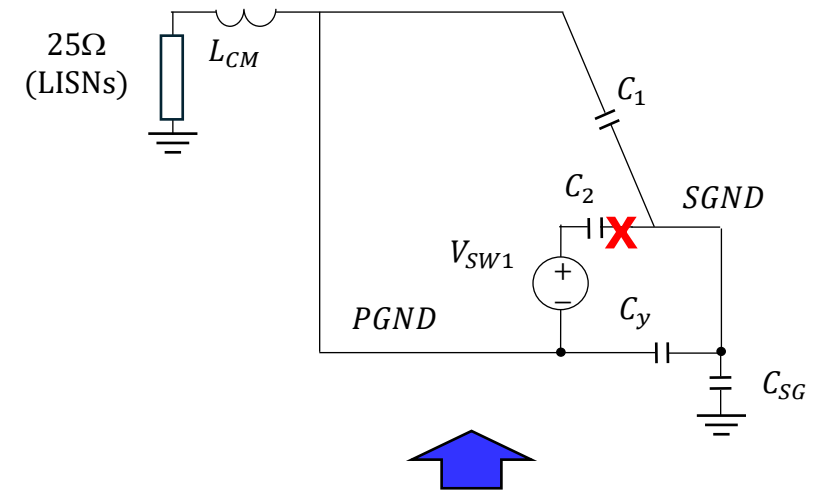
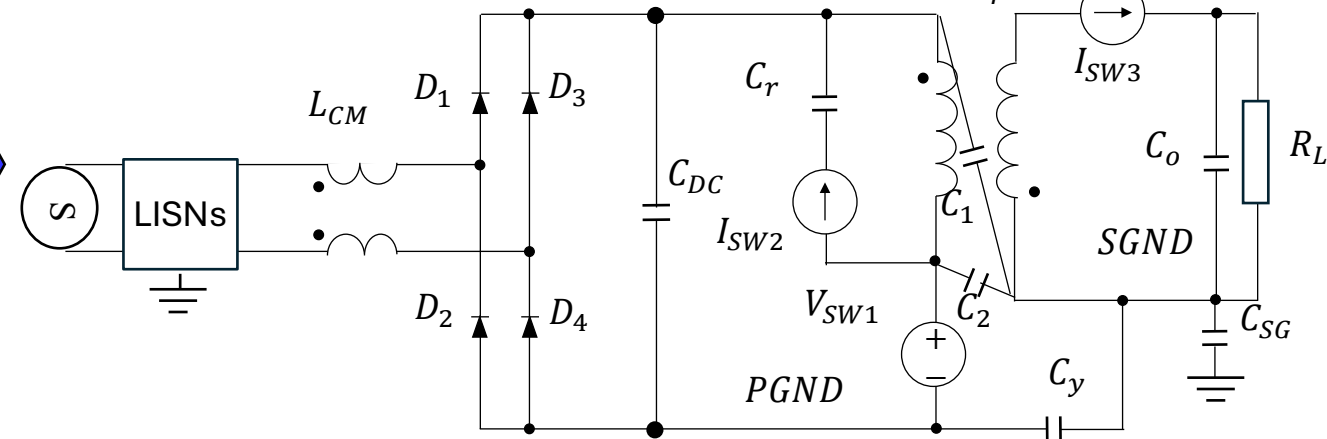
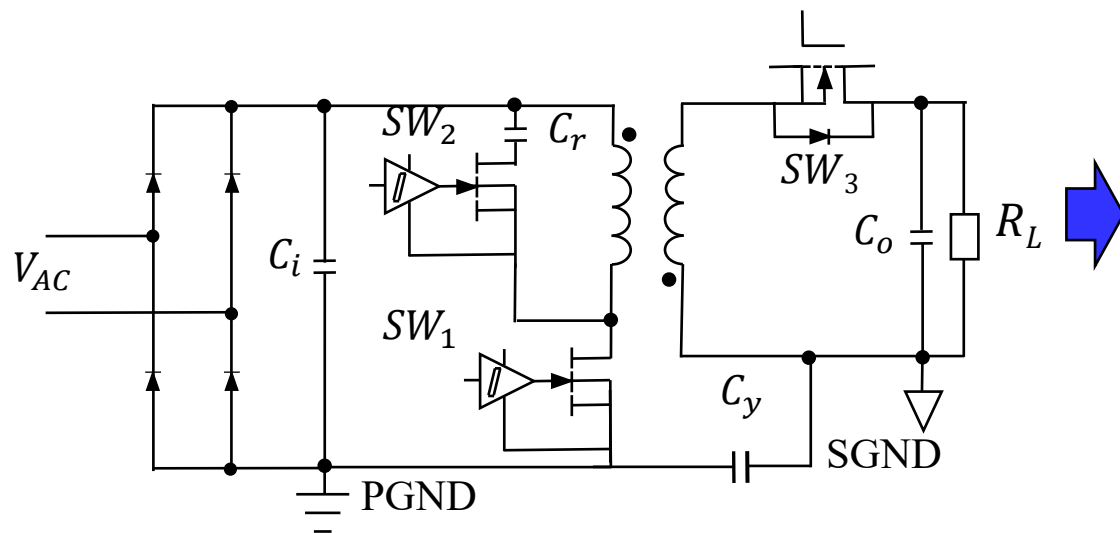
CM EMI Noise due to Switching Transformers

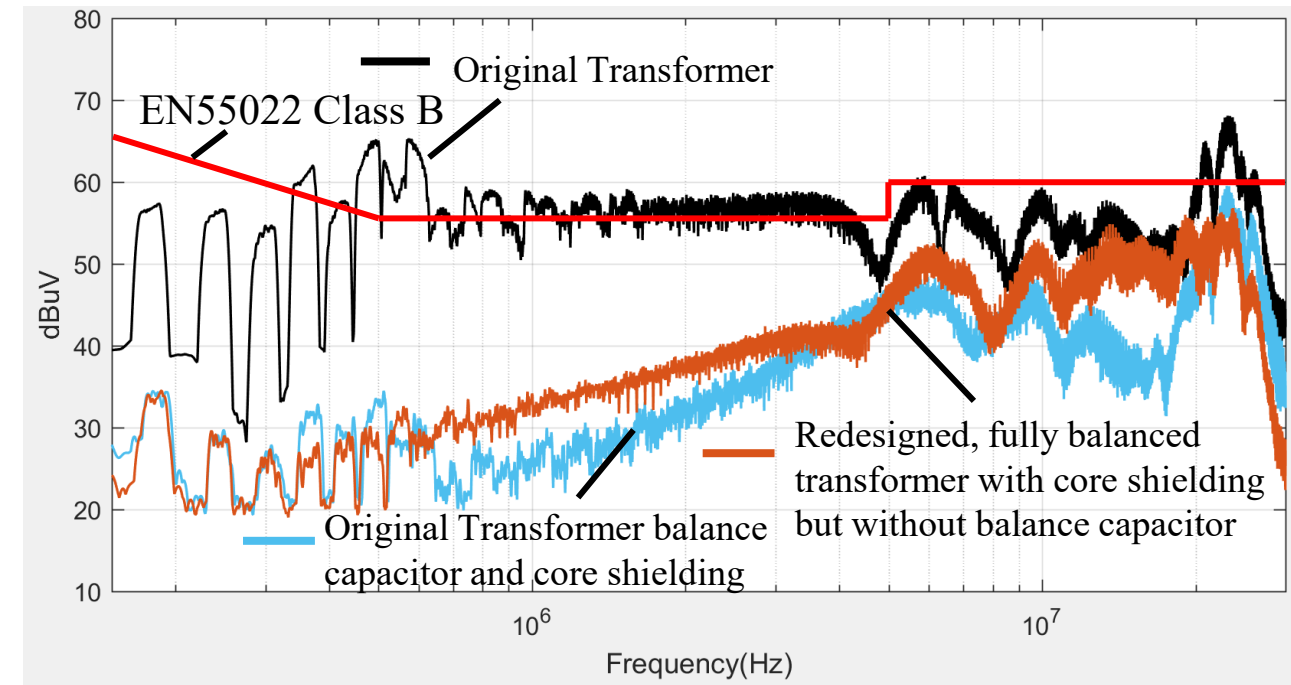
[4] Y. Li, H. Zhang, S. Wang, H. Sheng, C. P. Chng, and S. Lakshmikanthan, "Investigating Switching Transformers for Common Mode EMI Reduction to Remove Common Mode EMI Filters and Y-Capacitors in Flyback Converters," *IEEE Journal of Emerging and Selected Topics in Power Electronics*, vol. 6, no. 4, pp. 2287-2301, 2018

CM EMI Model of Switching Transformers



[5] H. Zhang, S. Wang, Y. Li, Q. Wang and D. Fu, "Two-Capacitor Transformer Winding Capacitance Models for Common-Mode EMI Noise Analysis in Isolated DC-DC Converters," in *IEEE Transactions on Power Electronics*, vol. 32, no. 11, pp. 8458-8469, Nov. 2017.





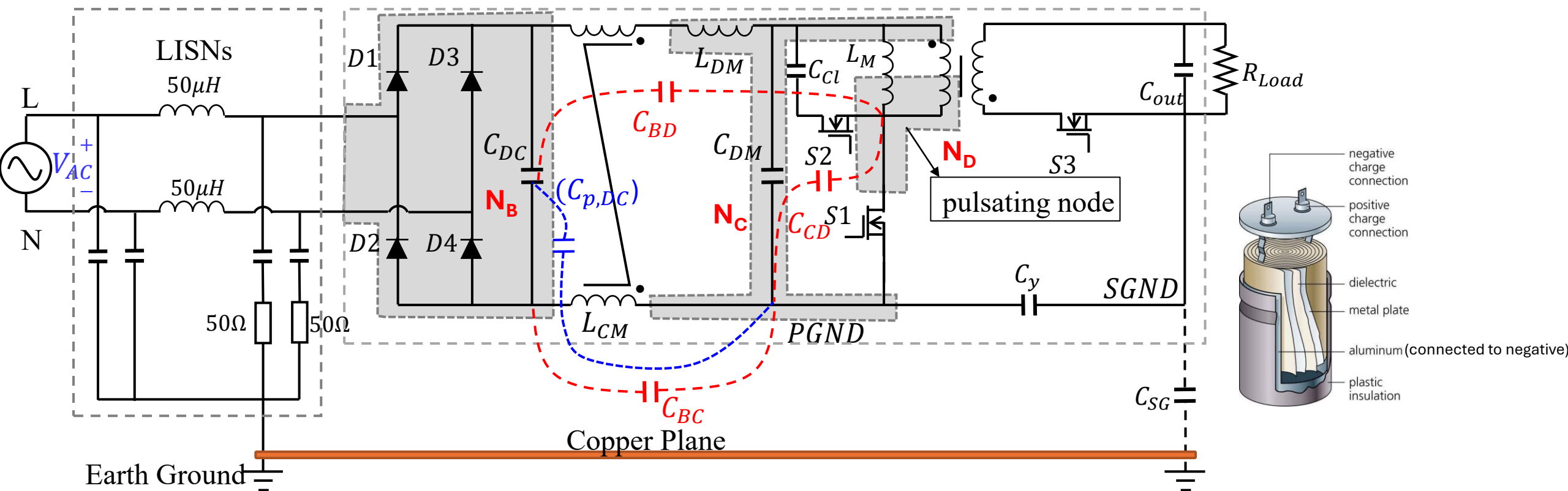
1. The adjacent windings between the primary and secondary should have small voltage difference
2. A cancellation winding can be used to generate reverse currents to cancel CM currents
3. An external cancellation capacitor can be used across primary and secondary to cancel CM currents

CM EMI Noise due to Near Electric Field Couplings

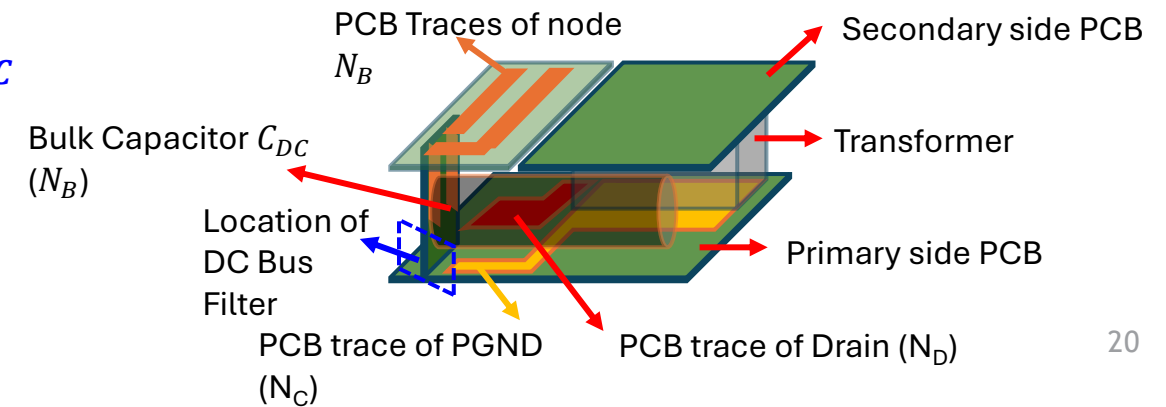
[6] Y. Li, S. Wang, H. Sheng and S. Lakshmikanthan, "Investigate and Reduce Capacitive Couplings in a Flyback Adapter With a DC-Bus Filter to Reduce EMI," in *IEEE Transactions on Power Electronics*, vol. 35, no. 7, pp. 6963-6973, July 2020

A Flyback Converter with A DC Bus Filter

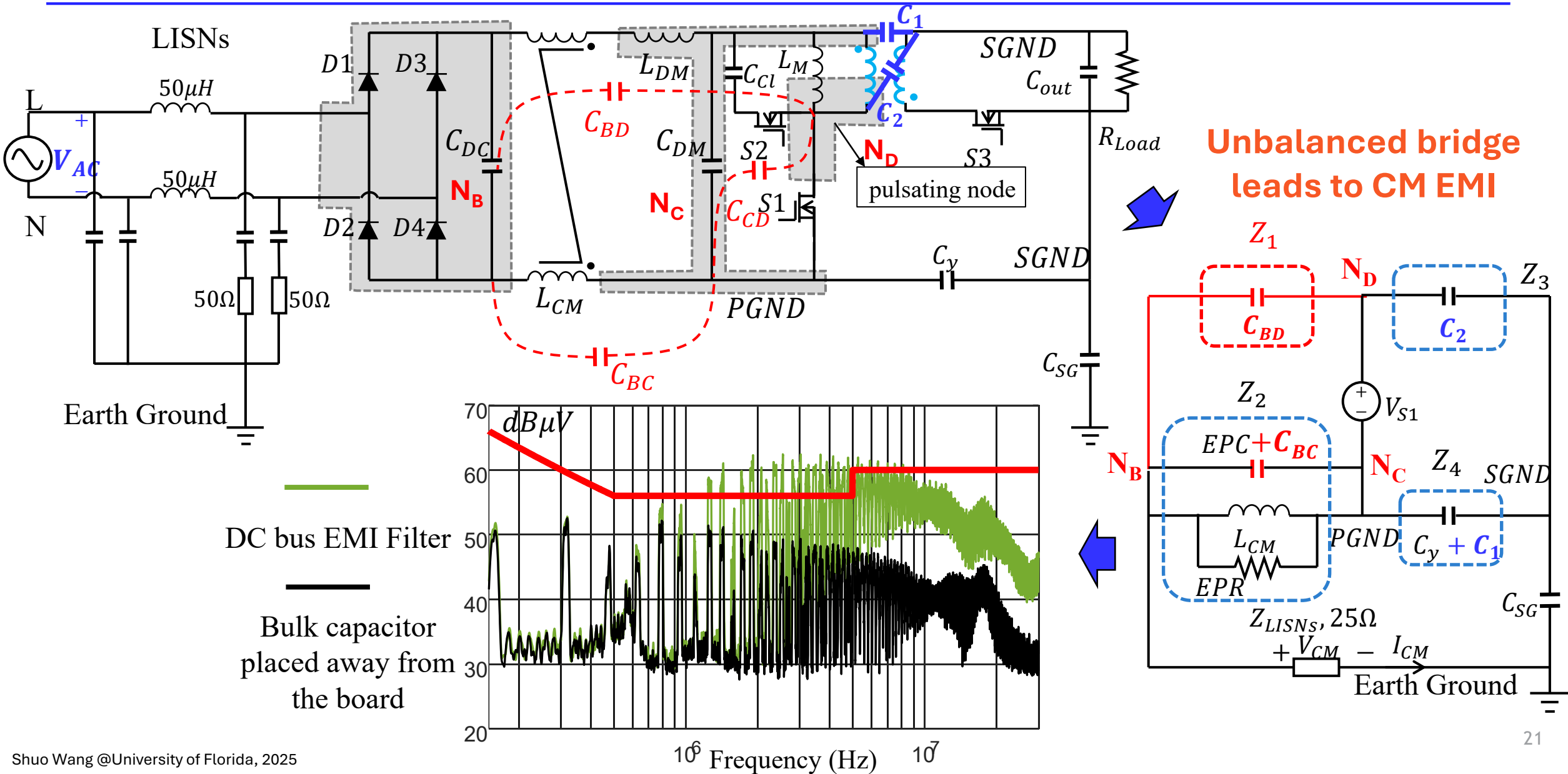
(Coupling with the Electrolytic Capacitor's Metal Shell)



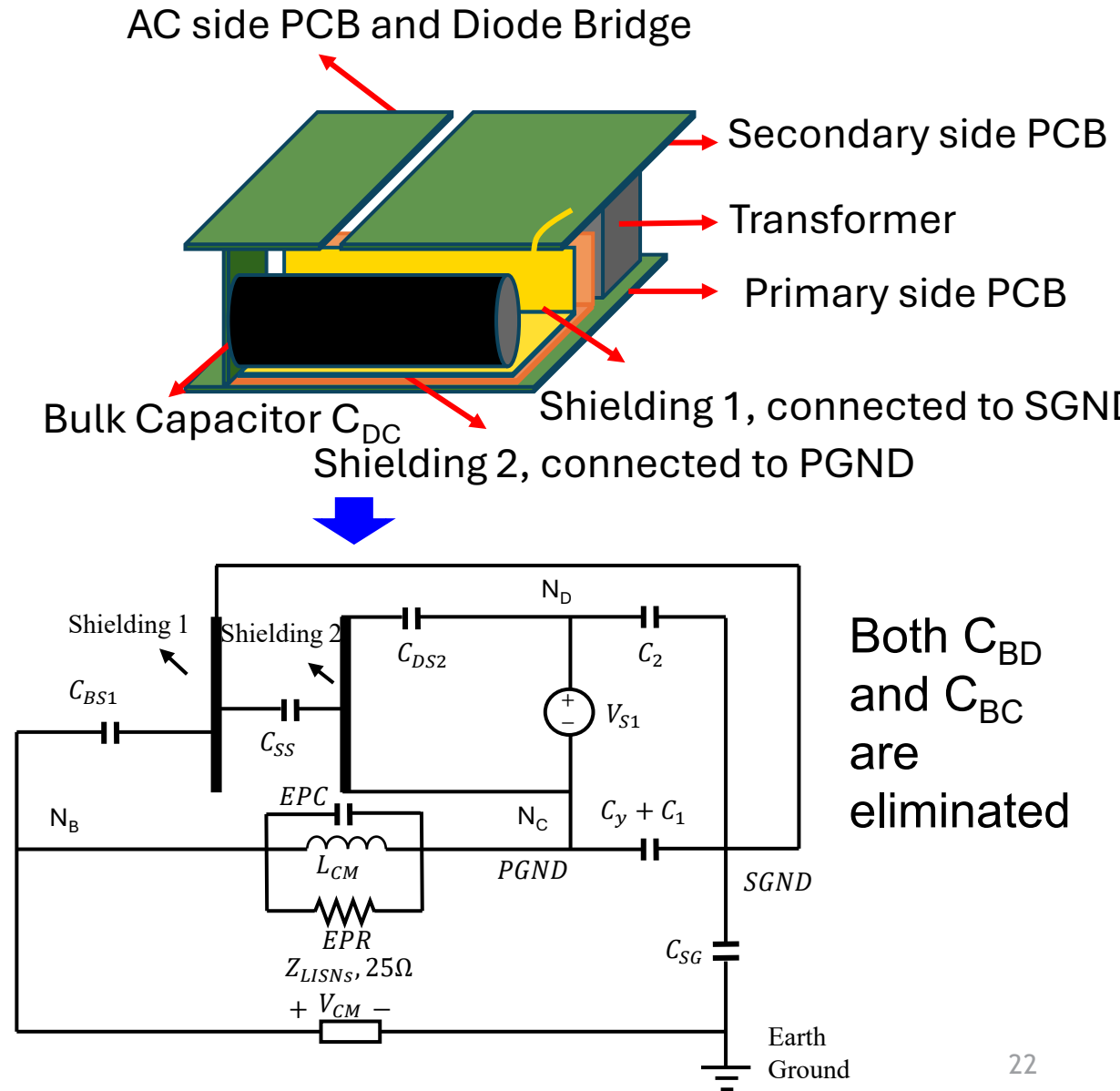
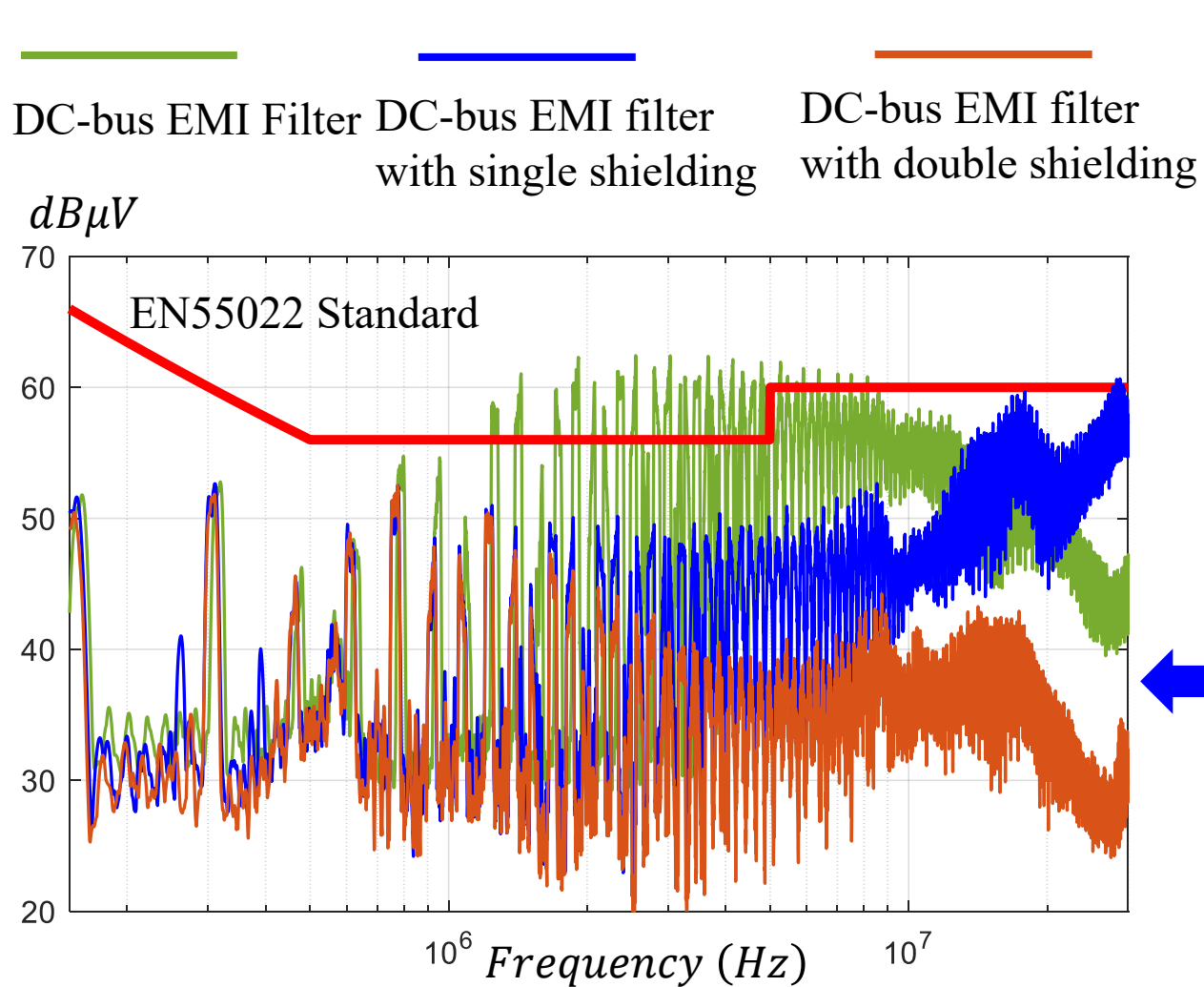
Electrolytic capacitor's metal shell couples to N_C : $C_{p,DC}$
It bypasses L_{CM} and can be combined with C_{BC} .



Near Electric Field Couplings Lead to High CM EMI



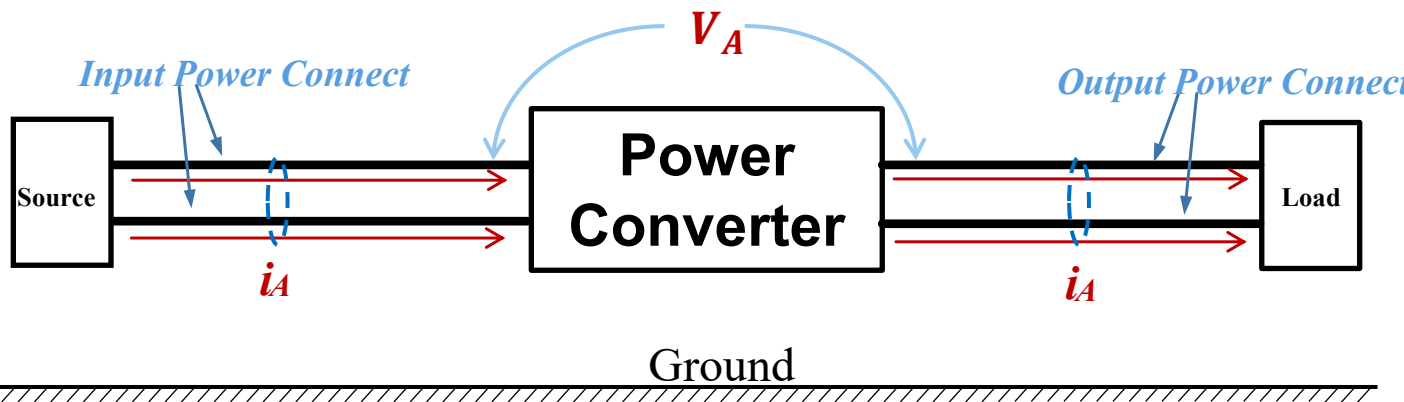
EMI Reduction by Shielding the DC Capacitor



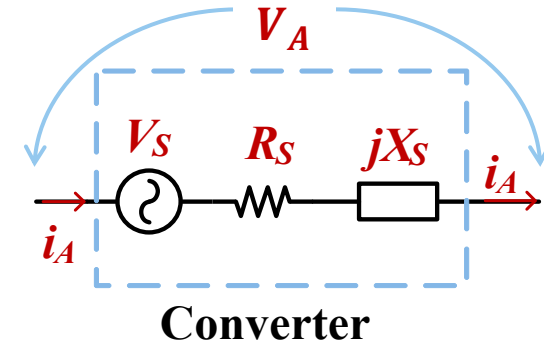
Radiated EMI of A Flyback Converter

[7] J. Yao, Y. Li, S. Wang, X. Huang, and X. Lyu, "Modeling and Reduction of Radiated EMI in a GaN IC-Based Active Clamp Flyback Adapter," IEEE Transactions on Power Electronics, vol. 36, no. 5, pp. 5440-5449, May 2021.

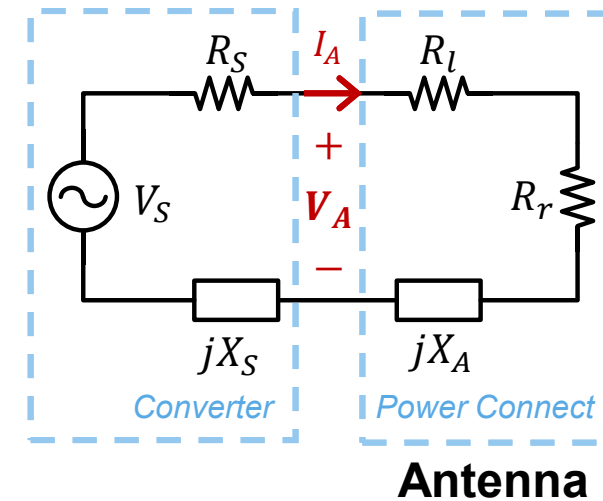
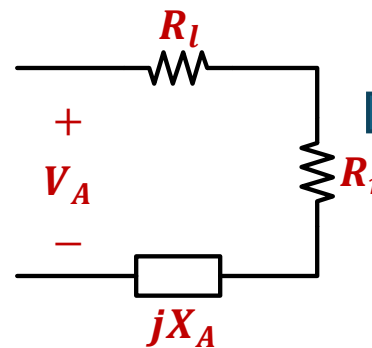
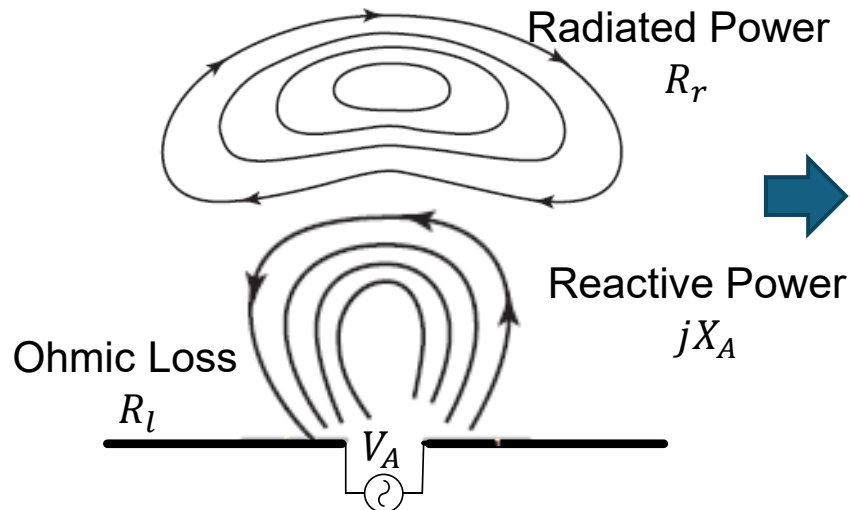
Radiated EMI Model for Power Converters with Input and Output Cables



Converter Thevenin Equivalence



Cables: Asymmetric dipole antenna:



$$E_{max} = \sqrt{\frac{R_r \eta D}{4\pi r^2}} \times |I_A|$$

$$= \sqrt{\frac{\eta D}{4\pi r^2}} \times |V_S|$$

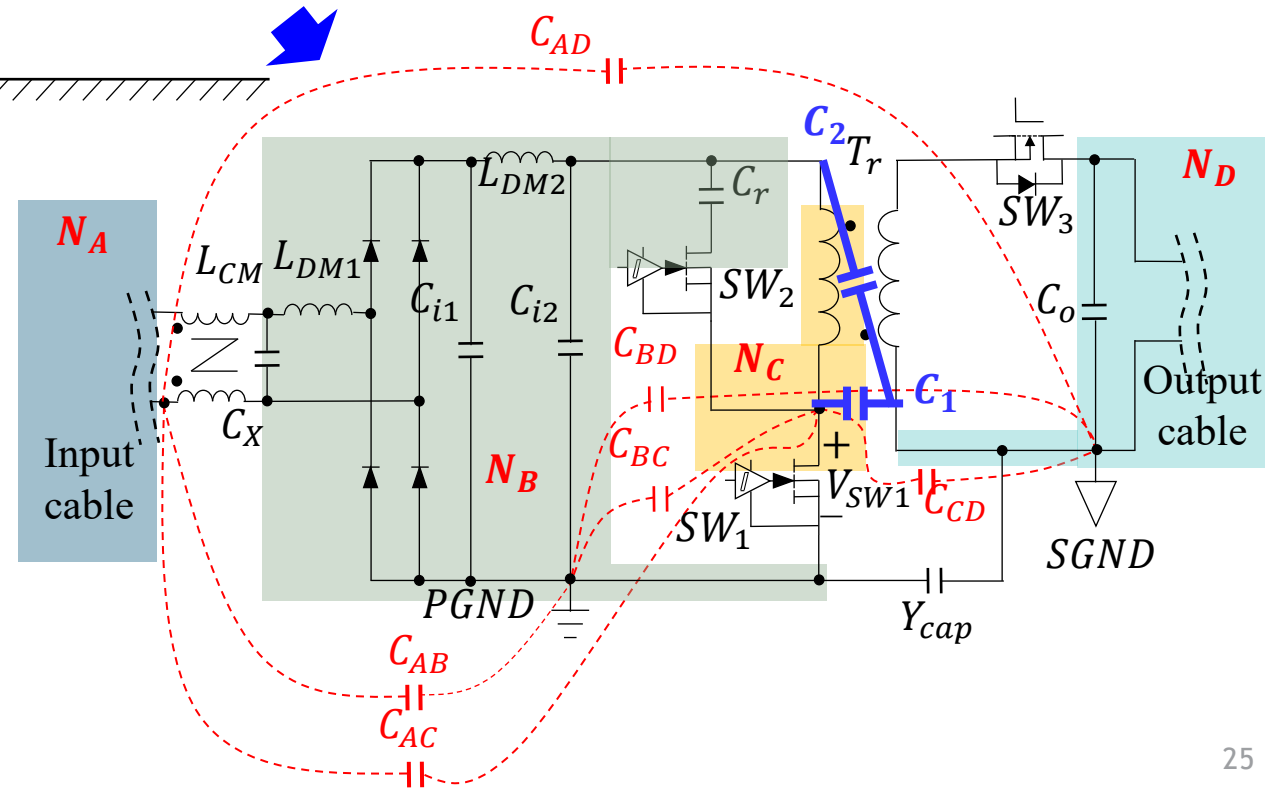
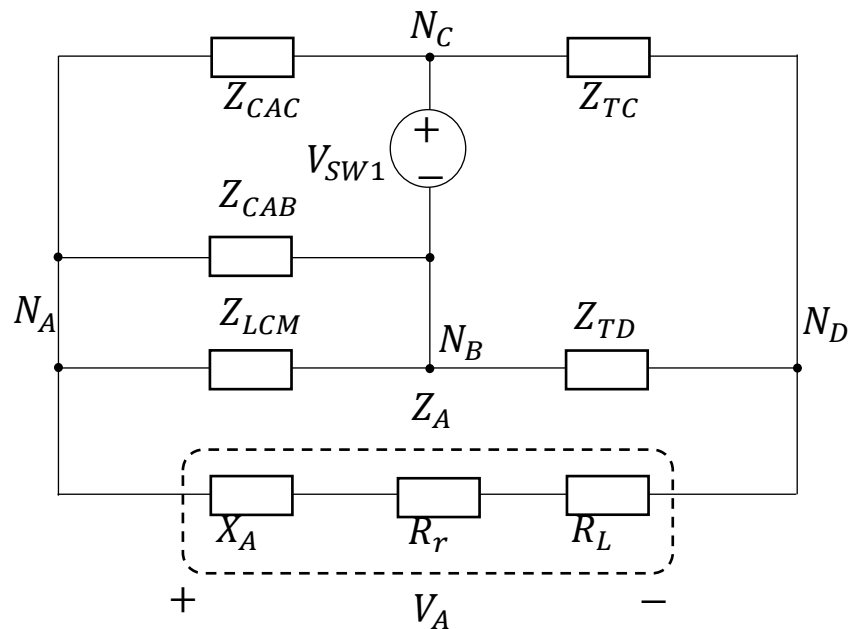
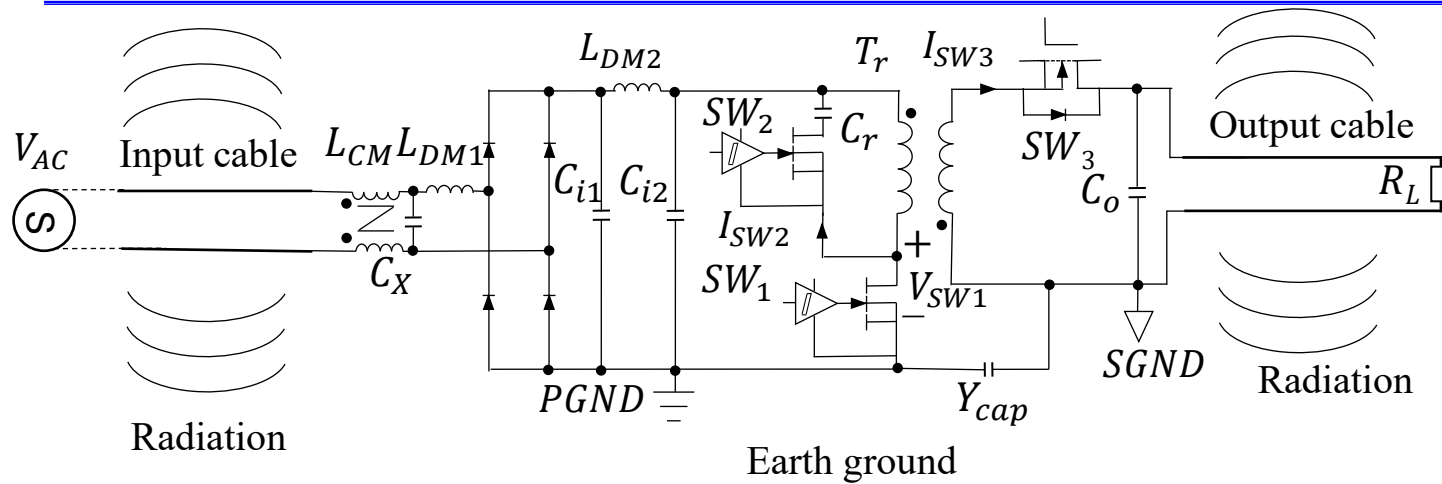
$$\times \frac{\sqrt{R_r}}{\sqrt{(R_S + R_r + R_l)^2 + (X_S + X_A)^2}}$$

Noise source

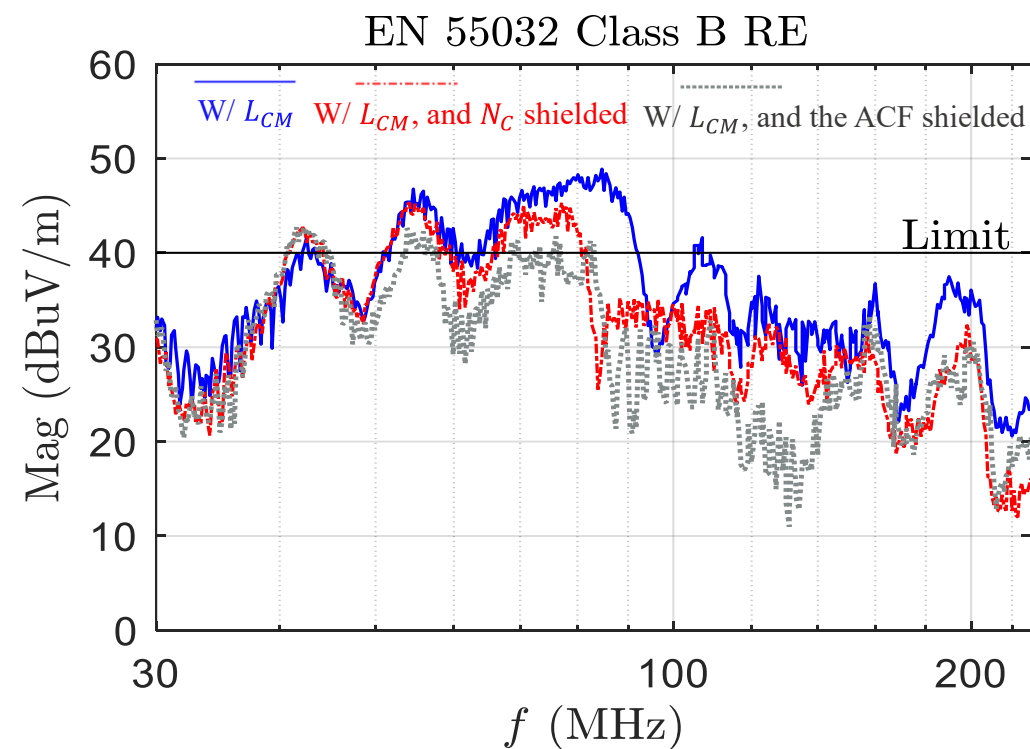
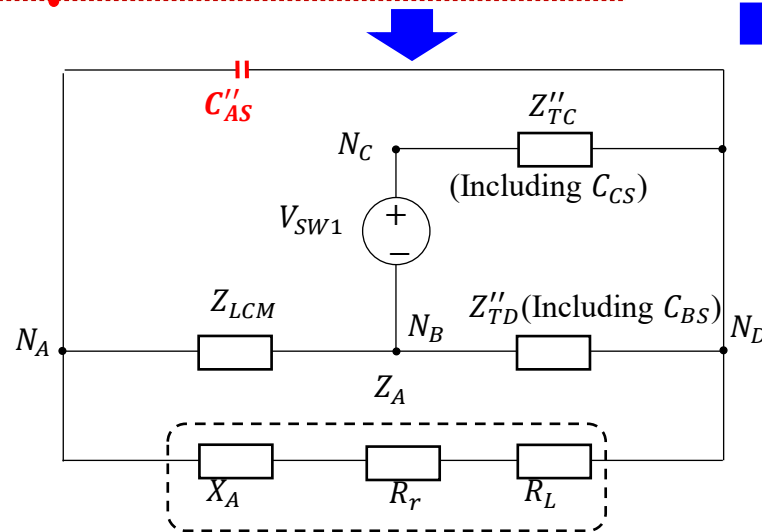
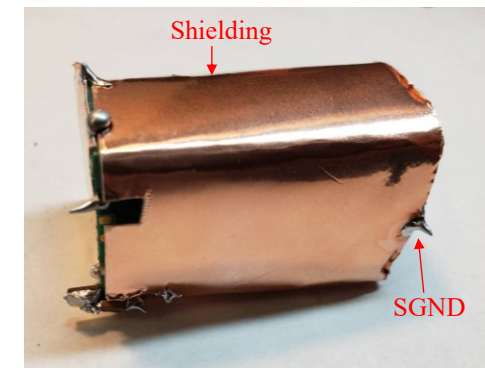
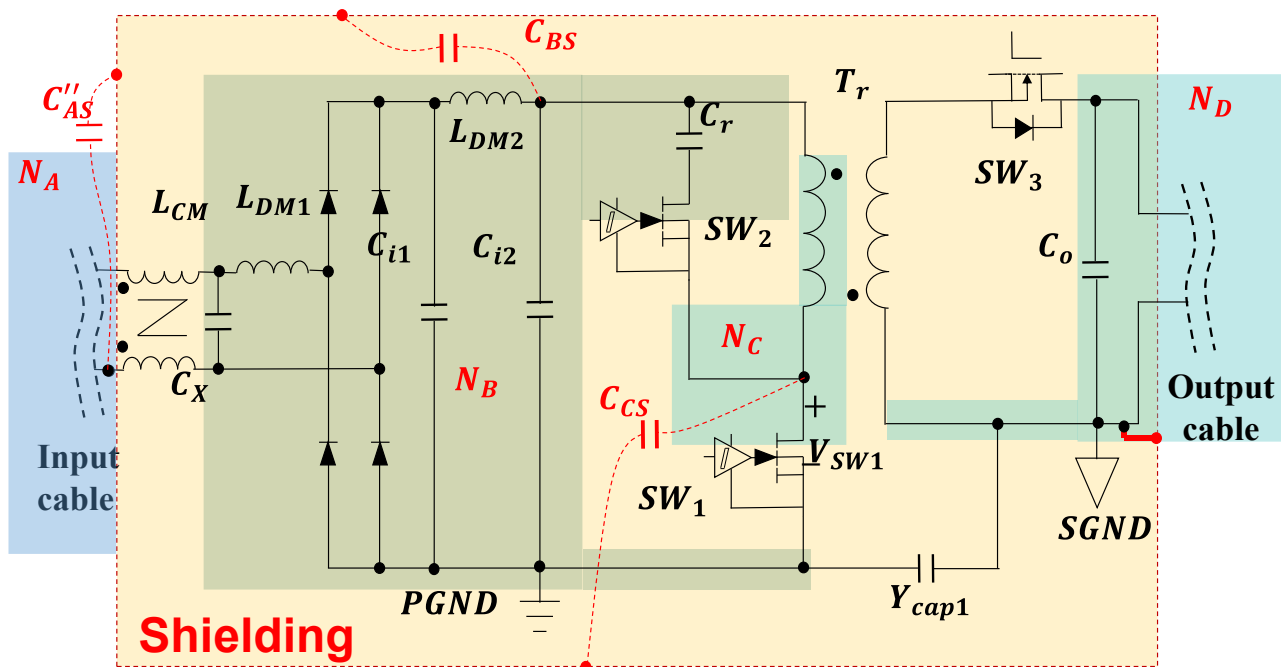
Due to impedances

[8]: Y. Zhang, S. Wang and Y. Chu, "Investigation of Radiated Electromagnetic Interference for an Isolated High-Frequency DC-DC Power Converter With Power Cables," in *IEEE Transactions on Power Electronics*, vol. 34, no. 10, pp. 9632-9643, Oct. 2019.

Radiated EMI Model of A Flyback Converter



Radiated EMI Reduction with A Shielding



Q & A

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